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(54) **METHODS AND APPARATUS FOR CHARACTERIZATION OF PETROLEUM FLUID EMPLOYING ANALYSIS OF HIGH MOLECULAR WEIGHT COMPONENTS**

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(58) **Field of Classification Search**

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USPC **702/6**
See application file for complete search history.

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Primary Examiner — Tung S Lau

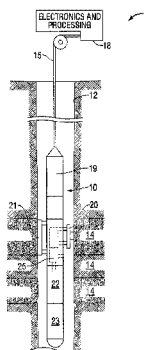
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(57) **ABSTRACT**

A methodology that performs downhole fluid analysis of fluid properties of a reservoir and characterizes the reservoir based upon such downhole fluid analysis. The methodology acquires at least one fluid sample at a respective measurement station and performs downhole fluid analysis to measure properties of the fluid sample, including concentration of a plurality of high molecular weight components. For each of a plurality of type classes corresponding to different subsets of a predetermined set of high molecular weight components, a model is used to predict the concentration of the components of the given type class for the plurality of measurement stations. The predicted concentrations of the high molecular weight components for the plurality of type classes are then compared with corresponding concentrations measured by downhole fluid analysis for the plurality of measurement stations to identify the best matching type class. The results of the comparison are used for reservoir analysis.

23 Claims, 9 Drawing Sheets



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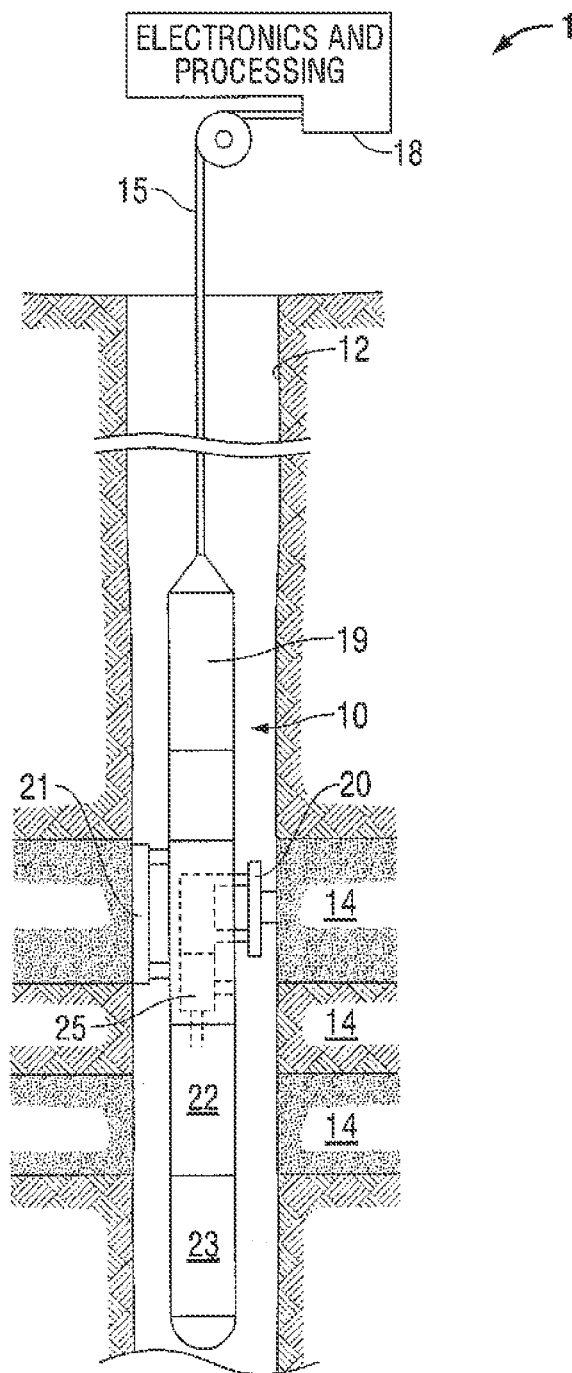


FIG. 1A

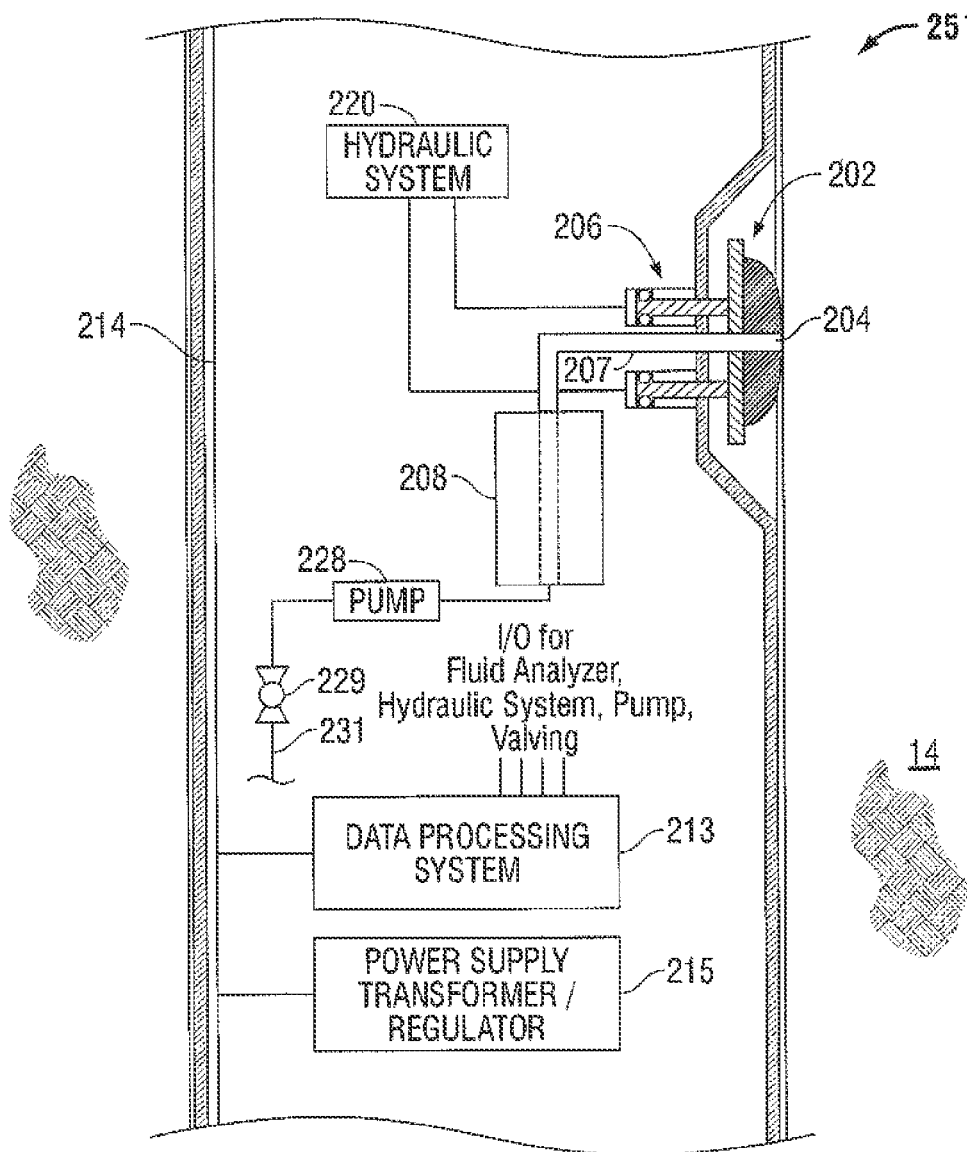


FIG. 1B

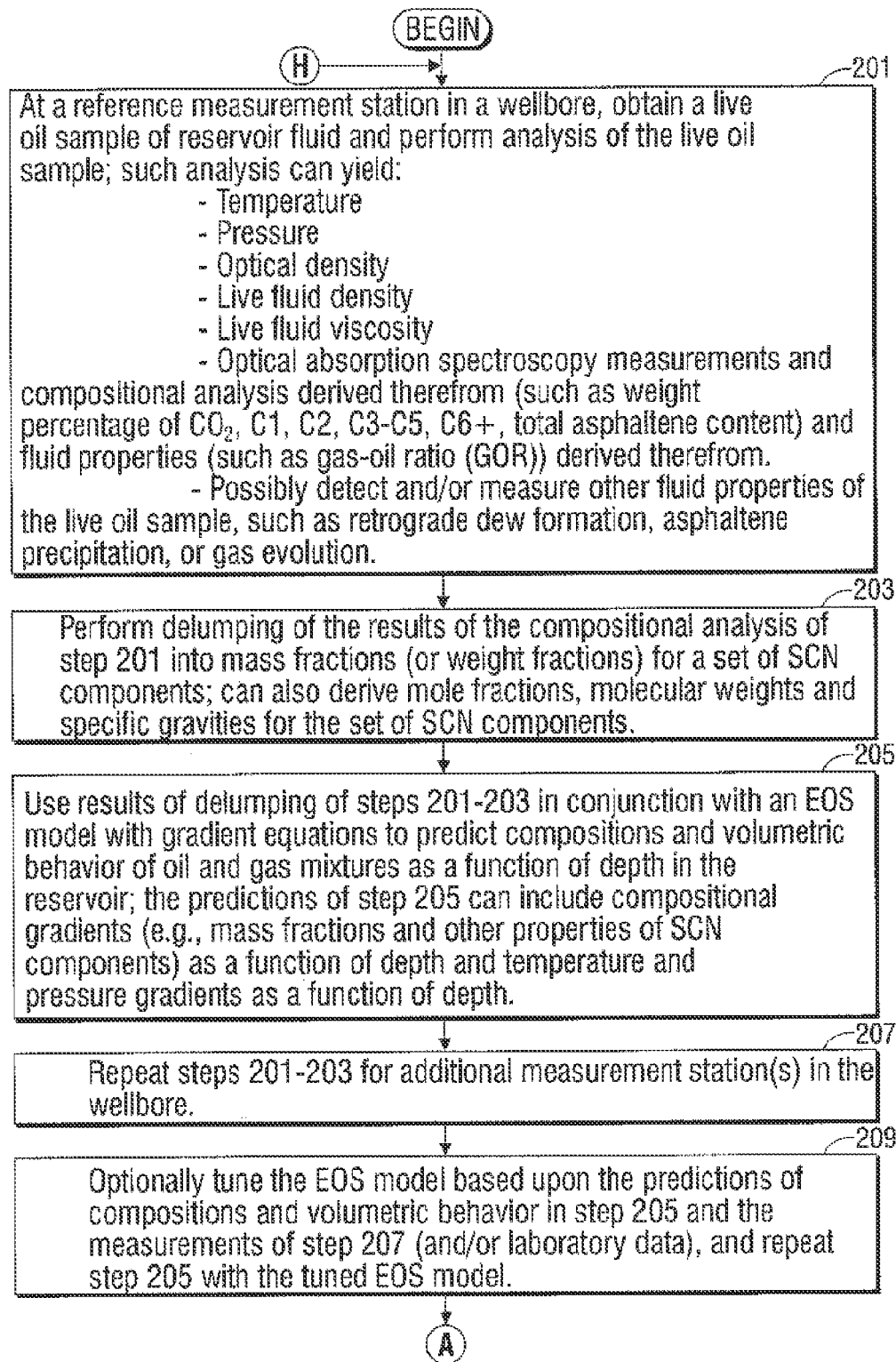


FIG. 2A

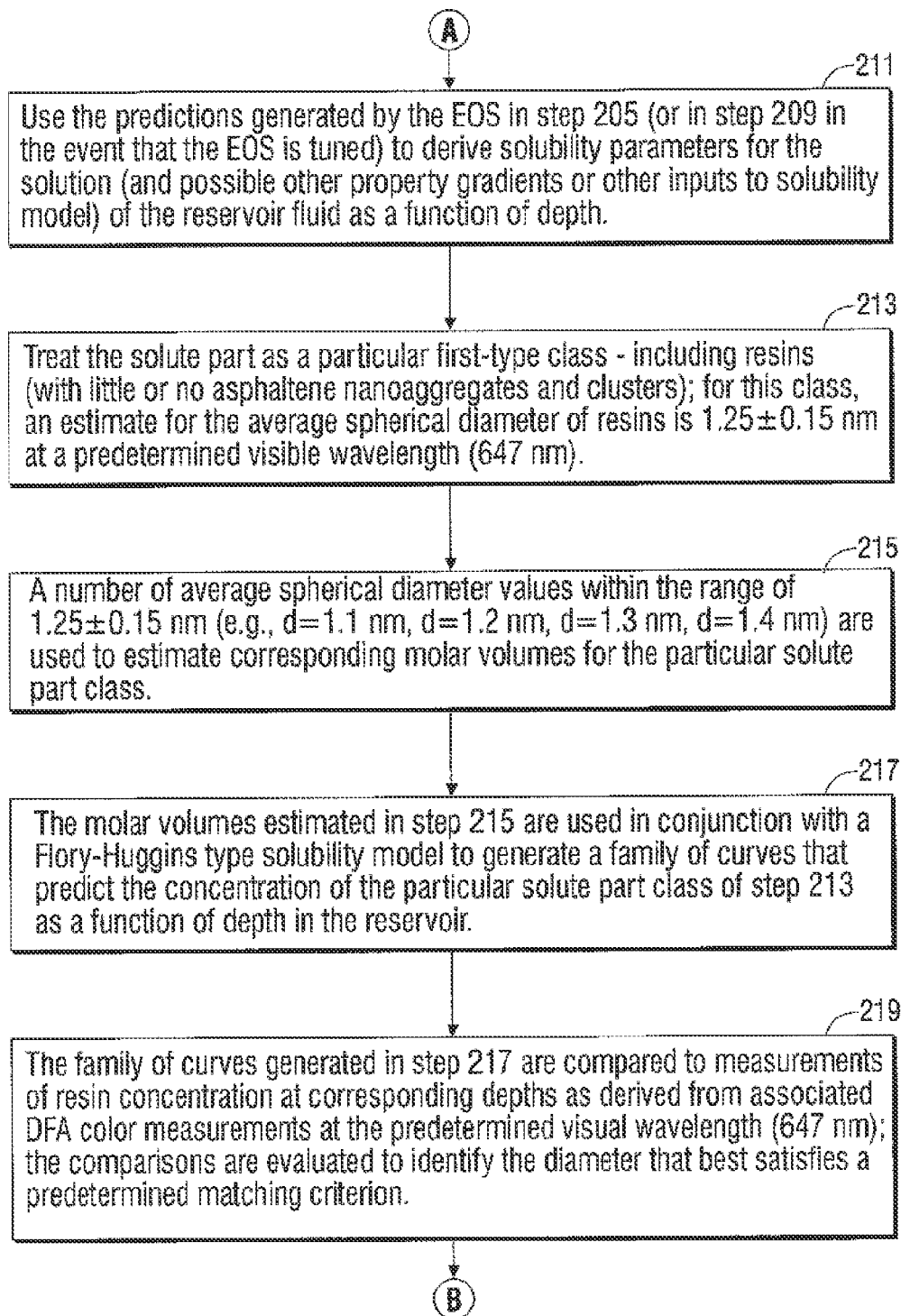


FIG. 2B

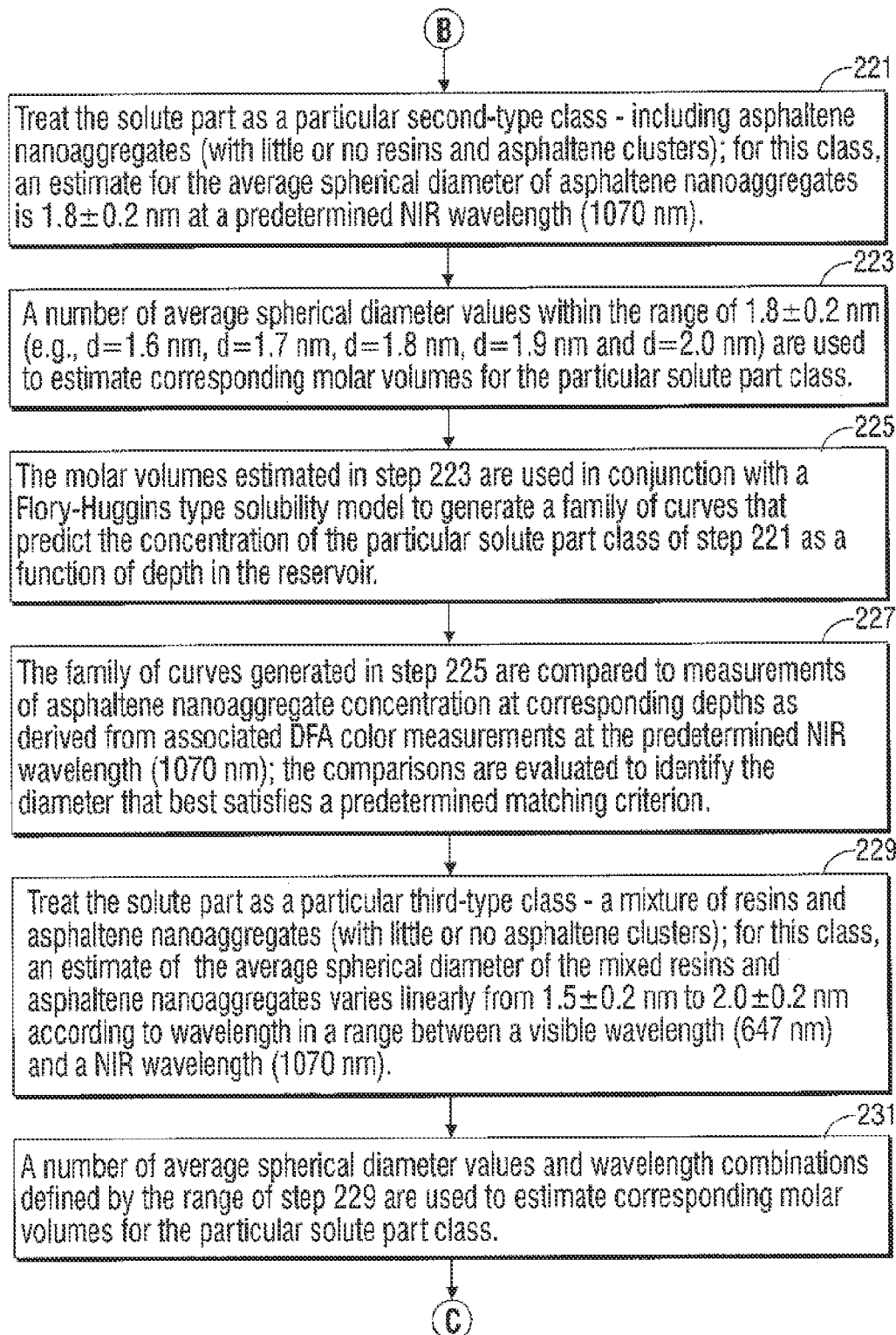


FIG. 2C

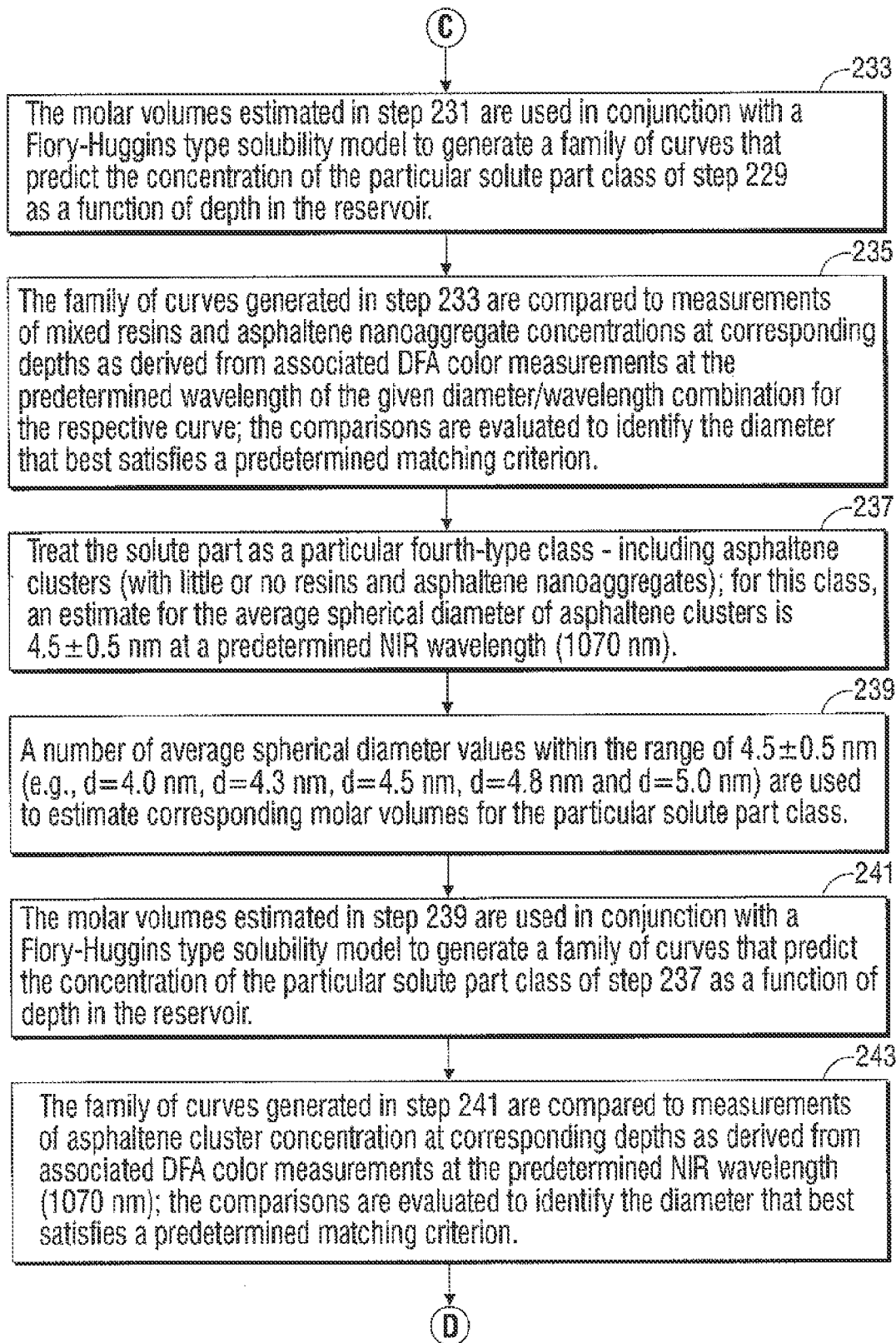


FIG. 2D

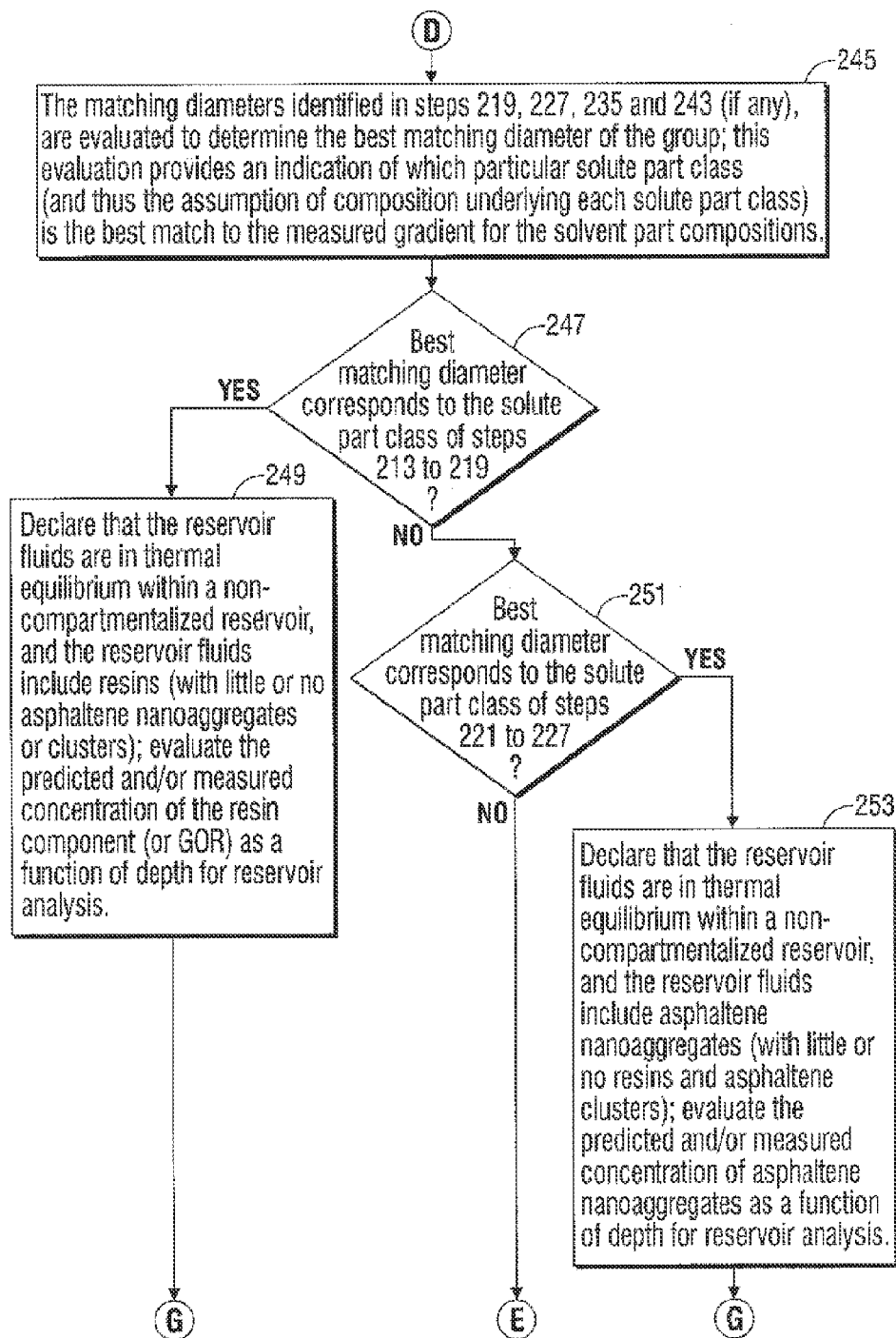


FIG. 2E

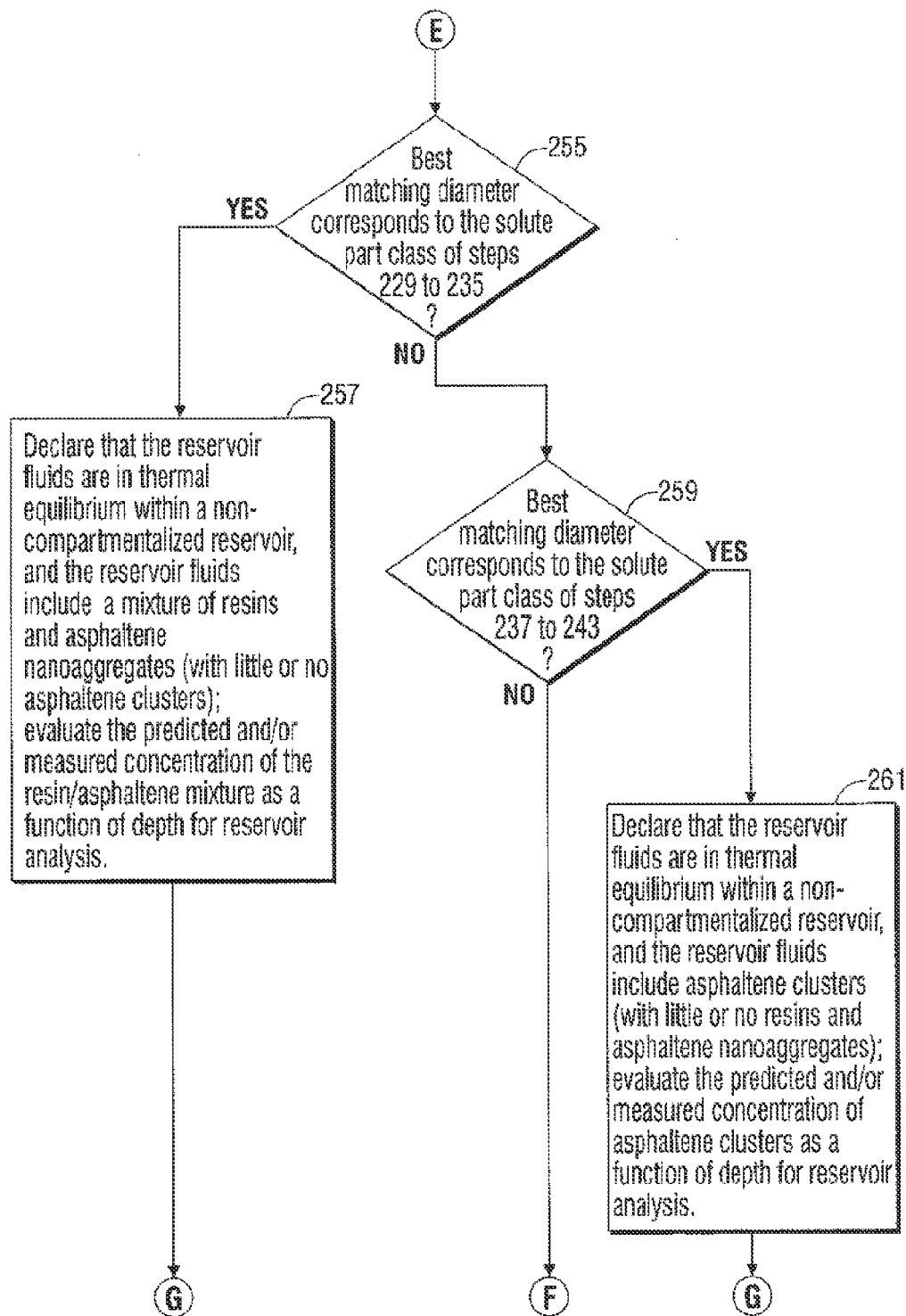


FIG. 2F

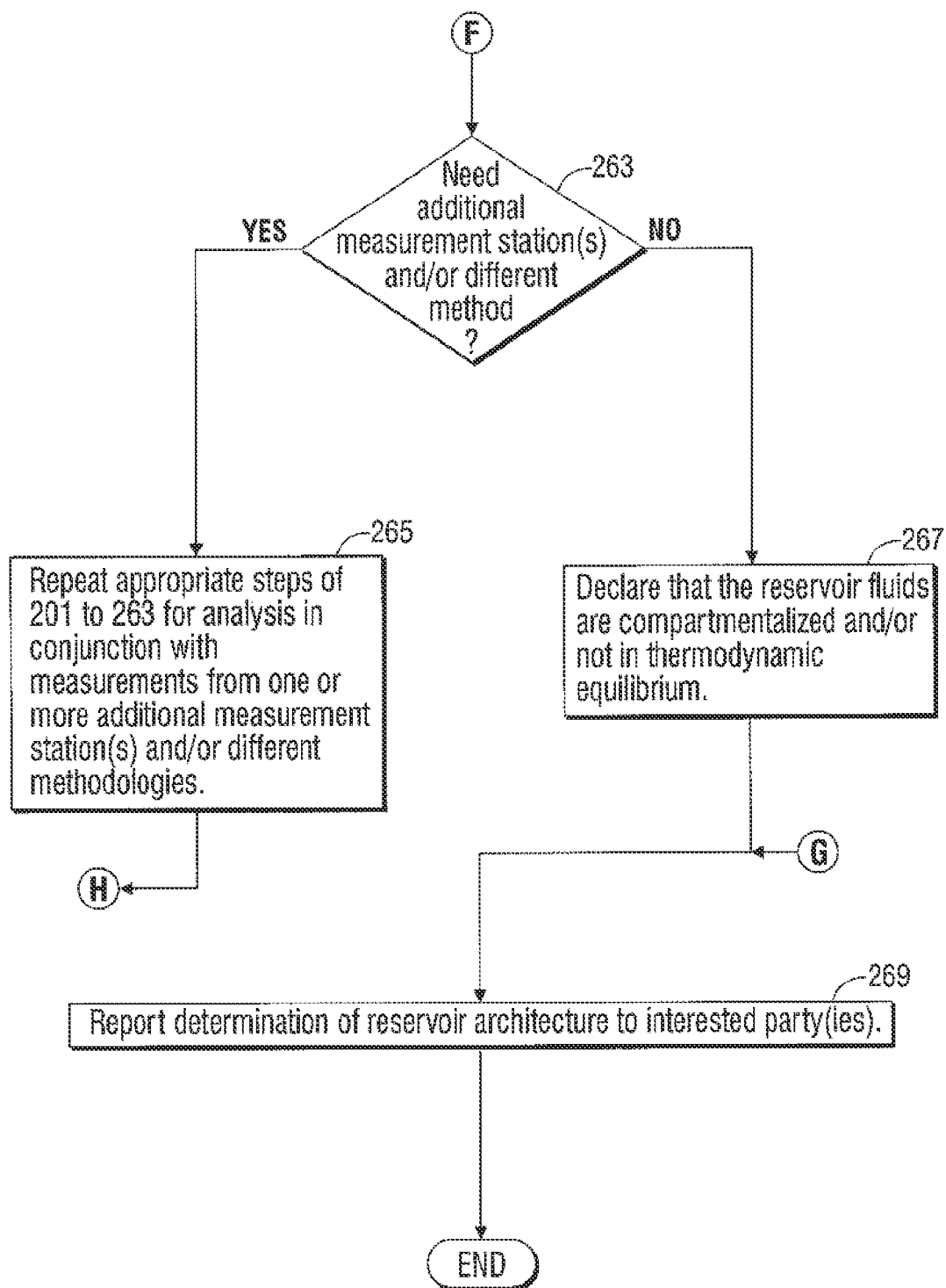


FIG. 2G

METHODS AND APPARATUS FOR CHARACTERIZATION OF PETROLEUM FLUID EMPLOYING ANALYSIS OF HIGH MOLECULAR WEIGHT COMPONENTS

CROSS-REFERENCE TO RELATED APPLICATIONS

The present invention claims priority from U.S. Provisional Patent Application 61/241,623, filed on Sep. 11, 2009, and U.S. Provisional Patent Application 61/314,505, filed on Mar. 16, 2010, both of which are herein incorporated by reference in their entireties.

BACKGROUND OF THE INVENTION

1. Field of the Invention

The present invention relates to methods and apparatus for characterizing petroleum fluids extracted from a hydrocarbon bearing geological formation. The invention has application to reservoir architecture understanding, although it is not limited thereto.

2. Description of Related Art

Petroleum consists of a complex mixture of hydrocarbons of various molecular weights, plus other organic compounds. The exact molecular composition of petroleum varies widely from formation to formation. The proportion of hydrocarbons in the mixture is highly variable and ranges from as much as 97 percent by weight in the lighter oils to as little as 50 percent in the heavier oils and bitumens. The hydrocarbons in petroleum are mostly alkanes (linear or branched), cycloalkanes, aromatic hydrocarbons, or more complicated chemicals like asphaltene. The other organic compounds in petroleum typically contain carbon dioxide (CO₂), nitrogen, oxygen and sulfur, and trace amounts of metals such as iron, nickel, copper and vanadium.

Petroleum is usually characterized by SARA fractionation where asphaltenes are removed by precipitation with a paraffinic solvent and the deasphalted oil separated into saturates, aromatics and resins by chromatographic separation.

The saturates include alkanes and cycloalkanes. The alkanes, also known as paraffins, are saturated hydrocarbons with straight or branched chains which contain only carbon and hydrogen and have the general formula C_nH_{2n+2}. They generally have from 5 to 40 carbon atoms per molecule, although shorter or longer molecules may be present in the mixture. The alkanes include methane (CH₄), ethane (C₂H₆), propane (C₃H₈), i-butane (iC₄H₁₀), n-butane (nC₄H₁₀), i-pentane (iC₅H₁₂), n-pentane (nC₅H₁₂), hexane (C₆H₁₄), heptane (C₇H₁₆), octane (C₈H₁₈), nonane (C₉H₂₀), decane (C₁₀H₂₂), hendecane (C₁₁H₂₄)—also referred to as undecane or undecane, dodecane (C₁₂H₂₆), tridecane (C₁₃H₂₈), tetradecane (C₁₄H₃₀), pentadecane (C₁₅H₃₂) and hexadecane (C₁₆H₃₄). The cycloalkanes, also known as naphthenes, are saturated hydrocarbons which have one or more carbon rings to which hydrogen atoms are attached according to the formula C_nH_{2n}. Cycloalkanes have similar properties to alkanes but have higher boiling points. The cycloalkanes include cyclopropane (C₃H₆), cyclobutane (C₄H₈), cyclopentane (C₅H₁₀), cyclohexane (C₆H₁₂), cycloheptane (C₇H₁₄), etc.

The aromatic hydrocarbons are unsaturated hydrocarbons which have one or more planar six-carbon rings called benzene rings, to which hydrogen atoms are attached with the formula C_nH_n. They tend to burn with a sooty flame, and many have a sweet aroma. The aromatic hydrocarbons include benzene (C₆H₆) and derivatives of benzene, as well as polyaromatic hydrocarbons.

Resins are the most polar and aromatic species present in the deasphalted oil and, it has been suggested, contribute to the enhanced solubility of asphaltenes in crude oil by solvating the polar and aromatic portions of the asphaltene molecules and aggregates.

Asphaltenes are insoluble in n-alkanes (such as n-pentane or n-heptane) and soluble in toluene. The C:H ratio is approximately 1:1.2, depending on the asphaltene source. Unlike most hydrocarbon constituents, asphaltenes typically contain a few percent of other atoms (called heteroatoms), such as sulfur, nitrogen, oxygen, vanadium, and nickel. Heavy oils and tar sands contain much higher proportions of asphaltenes than do medium-API oils or light oils. Condensates are virtually devoid of asphaltenes. As far as asphaltene structure is concerned, experts agree that some of the carbon and hydrogen atoms are found in ring-like, aromatic groups, which also contain the heteroatoms. Alkane chains and cyclic alkanes contain the rest of the carbon and hydrogen atoms and are linked to the ring groups. Within this framework, asphaltenes exhibit a range of molecular weight and composition. Asphaltenes have been shown to have a distribution of molecular weight in the range of 300 to 1400 g/mol with an average, of about 750 g/mol. This is compatible with a molecule containing seven or eight fused aromatic rings, and the range accommodates molecules with four to ten rings.

It is also known that asphaltene molecules aggregate to form nanoaggregates and clusters. The aggregation behavior depends on the solvent type. Laboratory studies have been conducted with asphaltene molecules dissolved in a solvent such as toluene. At extremely low concentrations (below 10⁻⁴ mass fraction), asphaltene molecules are dispersed as a true solution. At higher concentrations (on the order of 10⁻⁴ mass fraction), the asphaltene molecules stick together to form nanoaggregates. These nanoaggregates are dispersed in the fluid as a nanocolloid, meaning the nanometer-sized asphaltene particles are stably suspended in the continuous liquid phase solvent. At even higher concentrations (on the order of 5×10⁻³ mass fraction), the asphaltene nanoaggregates form clusters that remain stable as a colloid suspended in the liquid phase solvent. At higher concentrations (on the order of 5×10⁻² mass fraction), the asphaltene clusters flocculate to form clumps which precipitate out of the toluene solvent. In crude oil, asphaltenes exhibit a similar aggregation behavior. However, at the higher concentrations (on the order of 5×10⁻² mass fraction) that cause asphaltene clusters to flocculate in toluene, stability can continue such that the clusters form a viscoelastic network.

Computer-based modeling and simulation techniques have been developed for estimating the properties and/or behavior of petroleum fluids in a reservoir of interest. Typically, such techniques employ an equation of state (EOS) model that represents the phase behavior of the petroleum fluid in the reservoir. Once the EOS model is defined, it can be used to compute a wide array of properties of the petroleum fluid of the reservoir, such as: gas-oil ratio (GOR) or condensate-gas ratio (CGR), density of each phase, volumetric factors and compressibility, heat capacity and saturation pressure (bubble or dew point). Thus, the EOS model can be solved to obtain saturation pressure at a given temperature. Moreover, GOR, CGR, phase densities, and volumetric factors are byproducts of the EOS model. Transport properties, such as heat capacity or viscosity, can be derived from properties obtained from the EOS model, such as fluid composition. Furthermore, the EOS model can be extended with other reservoir evaluation techniques for compositional simulation of flow and production behavior of the petroleum fluid of the reservoir, as is well known in the art. For example, compositional simulations can

be helpful in studying (1) depletion of a volatile oil or gas condensate reservoir where phase compositions and properties vary significantly with, pressure below bubble or dew point pressures, (2) injection of non-equilibrium gas (dry or enriched) into a black oil reservoir to mobilize oil by vaporization into a more mobile gas phase or by condensation through an outright (single-contact) or dynamic (multiple-contact) miscibility, and (3) injection of carbon dioxide into an oil reservoir to mobilize oil by miscible displacement and by oil viscosity reduction and oil swelling.

In the past few decades, fluid homogeneity in a hydrocarbon reservoir has been assumed. However, there is now a growing awareness that fluids are often heterogeneous or compartmentalized in the reservoir. A compartmentalized reservoir consists of two or more compartments that effectively are not in hydraulic communication. Two types of reservoir compartmentalization have been identified, namely vertical and lateral compartmentalization. Vertical compartmentalization usually occurs as a result of faulting or stratigraphic changes in the reservoir, while lateral compartmentalization results from barriers to horizontal flow.

Molecular and thermal diffusion, natural convection, biodegradation, adsorption, and external fluxes can also lead to non-equilibrium hydrocarbon distribution in a reservoir.

Reservoir compartmentalization, as well as non-equilibrium hydrocarbon distribution, can significantly hinder production and can make the difference between an economically viable field and an economically nonviable field. Techniques to aid an operator to accurately describe reservoir compartments and their distribution, as well as non-equilibrium hydrocarbon distribution, can increase understanding of such reservoirs and ultimately raise production.

Conventionally, reservoir architecture (i.e., reservoir compartmentalization as well as non-equilibrium hydrocarbon distribution) has been determined utilizing pressure-depth plots and pressure gradient analysis with traditional straight-line regression schemes. This process may, however, be misleading as fluid compositional changes and compartmentalization give distortions in the pressure gradients, which result in erroneous interpretations of fluid contacts or pressure seals. Additionally, pressure communication does not prove flow connectivity.

U.S. Patent Application Publication 2009/0312997 provides a methodology for correlating composition data of live oil measured using a downhole fluid analyzer tool with predicted composition data to determine whether asphaltenes are in an equilibrium distribution within the reservoir. The methodology treats asphaltenes within the framework of polymer solution theory (Flory-Huggins model). The methodology generates a family of curves that predicts asphaltene content as a function of depth. The curves can be viewed as a function of two parameters, the volume and solubility of the asphaltene. The curves can be fit to measured asphaltene content as derived from the downhole fluid analysis tool. There can be uncertainty in the fitting process as asphaltene volume can vary widely. In these instances, it can be difficult to assess the accuracy of the Flory-Huggins model and the resulting determinations based thereon at any given time, and thus know whether or not there is a need to acquire and analyze more downhole samples in order to refine or tune the Flory-Huggins model and the resulting determinations based thereon.

BRIEF SUMMARY OF THE INVENTION

It is therefore an object of the invention to provide methods and apparatus that accurately characterize compositional components and fluid properties at varying locations in a

reservoir in order to allow for accurate reservoir architecture analysis (e.g., detection of connectivity (or compartmentalization) and equilibrium (or non-equilibrium) hydrocarbon distribution in the reservoir of interest).

In accord with the objects of the invention, a downhole fluid analysis tool is employed to obtain and perform downhole fluid analysis of live oil samples at multiple measurement stations within a wellbore traversing a reservoir of interest. Such downhole fluid analysis measures compositional components and possibly other fluid properties of each live oil sample. The downhole measurements can be used in conjunction with an equation of state model to predict gradients of the compositional components as well as other fluid properties for reservoir analysis. A model is used to predict concentrations of a plurality of high molecular weight solute part type classes at varying locations in a reservoir. Such predictions are compared against the downhole measurements associated therewith to identify the best matching solute part type class for reservoir analysis. For example, the predicted or measured concentrations of the best matching solute part type class can be evaluated to determine that the reservoir is connected and in thermal equilibrium. Alternatively, if no match is found, the results can determine that the reservoir is compartmentalized or not in thermodynamic equilibrium. The results of the comparison can also be used to determine whether or not to include one or more additional measurement stations in the analysis workflow (and possibly refine or tune the models of the workflow based on the measurements for the additional measurement stations) for better accuracy and confidence in the fluid measurements and predictions that are used for the reservoir analysis.

In the preferred embodiment, the model is a Flory-Huggins type solubility model that characterizes relative concentrations of a set of high molecular weight components as a function of depth as related to relative solubility, density and molar volume of the high molecular weight components of the set at varying depth. The solubility model treats the reservoir fluid as a mixture of two parts, the two parts being a solute part and a solvent part, the solute part comprising the set of high molecular weight components. The high molecular weight components of the solute part are preferably selected from the group including resins, asphaltene nanoaggregates, and asphaltene clusters. Preferred embodiments of such models are set forth in detail below.

Additional objects and advantages of the invention will become apparent to those skilled in the art upon reference to the detailed description taken in conjunction with the provided figures.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1A is a schematic diagram of an exemplary petroleum reservoir analysis system in which the present invention is embodied.

FIG. 1B is a schematic diagram of an exemplary fluid analysis module suitable for use in the borehole tool of FIG. 1A.

FIGS. 2A-2G, collectively, are a flow chart of data analysis operations that includes downhole fluid measurements at a number of different measurement stations within a wellbore traversing a reservoir or interest in conjunction with at least one solubility model that characterizes the relationship between solvent and solute parts of the reservoir fluids at different measurement stations. The model is used to calculate a predicted value of the relative concentration of the solute part for at least one given measurement station for different solute type classes. A consistency check is per-

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formed that involves comparison of the predicted solute part concentration values with corresponding solute part concentration values measured by downhole fluid analysis. The results are used to determine the best matching solute type class. Reservoir architecture is determined based on the best matching solute type class.

DETAILED DESCRIPTION OF THE INVENTION

FIG. 1A illustrates an exemplary petroleum reservoir analysis system 1 in which the present invention is embodied. The system 1 includes a borehole tool 10 suspended in the borehole 12 from the lower end of a typical multiconductor cable 15 that is spooled in a usual fashion on a suitable winch on the formation surface. The cable 15 is electrically coupled to an electrical control system 18 on the formation surface. The tool 10 includes an elongated body 19 which carries a selectively extendable fluid admitting assembly 20 and a selectively extendable tool anchoring member 21 which are respectively arranged on opposite sides of the tool body 19. The fluid admitting assembly 20 is equipped for selectively sealing off or isolating selected portions of the wall of the borehole 12 such that fluid communication with the adjacent earth formation 14 is established. The fluid admitting assembly 20 and tool 10 include a flowline leading to a fluid analysis module 25. The formation fluid obtained by the fluid admitting assembly 20 flows through the flowline and through the fluid analysis module 25. The fluid may thereafter be expelled through a port or it may be sent to one or more fluid collecting chambers 22 and 23 which may receive and retain the fluids obtained from the formation. With the assembly 20 sealingly engaging the formation 14, a short rapid pressure drop can be used to break the mudcake seal. Normally, the first fluid drawn into the tool will be highly contaminated with mud filtrate. As the tool continues to draw fluid from the formation 14, the area near the assembly 20 cleans up and reservoir fluid becomes the dominant constituent. The time required for cleanup depends upon many parameters, including formation permeability, fluid viscosity, the pressure differences between the borehole and the formation, and overbalanced pressure difference and its duration during drilling. Increasing the pump rate can shorten the cleanup time, but the rate must be controlled carefully to preserve formation pressure conditions.

The fluid analysis module 25 includes means for measuring the temperature and pressure of the fluid in the flowline. The fluid analysis module 25 derives properties that characterize the formation fluid sample at the flowline pressure and temperature. In the preferred embodiment, the fluid analysis module 25 measures absorption spectra and translates such measurements into concentrations of several alkane components and groups in the fluid sample. In an illustrative embodiment, the fluid analysis module 25 provides measurements of the concentrations (e.g., weight percentages) of carbon dioxide (CO_2), methane (CH_4), ethane (C_2H_6), the C3-C5 alkane group, the lump of hexane and heavier alkane components (C6+), and asphaltene content. The C3-C5 alkane group includes propane, butane, and pentane. The C6+ alkane group includes hexane (C_6H_{14}), heptane (C_7H_{16}), octane (C_8H_{18}), nonane (C_9H_{20}), decane ($\text{C}_{10}\text{H}_{22}$), hendecane ($\text{C}_{11}\text{H}_{24}$)—also referred to as endecane or undecane, dodecane ($\text{C}_{12}\text{H}_{26}$), tridecane ($\text{C}_{13}\text{H}_{28}$), tetradecane ($\text{C}_{14}\text{H}_{30}$), pentadecane ($\text{C}_{15}\text{H}_{32}$), hexadecane ($\text{C}_{16}\text{H}_{34}$), etc. The fluid analysis module 25 also provides a means that measures live fluid density (ρ) at the flowline temperature and

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pressure, live fluid viscosity (μ) at flowline temperature and pressure (in cp), formation pressure, and formation temperature.

Control of the fluid admitting assembly 20 and fluid analysis module 25, and the flow path to the collecting chambers 22, 23 is maintained by the control system 18. As will be appreciated by those skilled in the art, the fluid analysis module 25 and the surface-located electrical control system 18 include data processing functionality (e.g., one or more microprocessors, associated memory, and other hardware and/or software) to implement the invention as described herein. The electrical control system 18 can also be realized by a distributed data processing system wherein data measured by the tool 10 is communicated (preferably in real time) over a communication link (typically a satellite link) to a remote location for data analysis as described herein. The data analysis can be carried out on a workstation or other suitable data processing system (such as a computer cluster or computing grid).

Formation fluids sampled by tire tool 10 may be contaminated with mud filtrate. That is, the formation fluids may be contaminated with the filtrate of a drilling fluid that seeps into the formation 14 during the drilling process. Thus, when fluids are withdrawn from the formation 14 by the fluid admitting assembly 20, they may include mud filtrate. In some examples, formation fluids are withdrawn from the formation 14 and pumped into the borehole or into a large waste chamber in the tool 10 until the fluid being withdrawn becomes sufficiently clean. A clean sample is one where the concentration of mud filtrate in the sample fluid is acceptably low so that the fluid substantially represents native (i.e., naturally occurring) formation fluids. In the illustrated example, the tool 10 is provided with fluid collecting chambers 22 and 23 to store collected fluid samples.

The system of FIG. 1A is adapted to make in situ determinations regarding hydrocarbon bearing geological formations by downhole sampling of reservoir fluid at one or more measurement stations within the borehole 12, conducting downhole fluid analysis of one or more reservoir fluid samples for each measurement station (including compositional analysis, such as estimating concentrations of a plurality of compositional components of a given sample, as well as other fluid properties), and relating the downhole fluid analysis to an equation of state (EOS) model of the thermodynamic behavior of the fluid in order to characterize the reservoir fluid at different locations within the reservoir. With the reservoir fluid characterized with respect to its thermodynamic behavior, fluid production parameters, transport properties, and other commercially useful indicators of the reservoir can be computed.

For example, the EOS model can provide the phase envelope that can be used to interactively vary the rate at which samples are collected in order to avoid entering the two-phase region. In another example, the EOS can provide useful properties in assessing production methodologies for the particular reserve. Such properties can include density, viscosity, and volume of gas formed from a liquid after expansion to a specified temperature and pressure. The characterization of the fluid sample with respect to its thermodynamic model can also be used as a benchmark to determine the validity of the obtained sample, whether to retain the sample, and/or whether to obtain another sample at the location of interest. More particularly, based on the thermodynamic model and information regarding formation pressures, sampling pressures, and formation temperatures, if it is determined that the fluid sample was obtained near or below the bubble line of the sample, a decision, may be made to jettison the sample and/or

to obtain a sample at a slower rate (i.e., a smaller pressure drop) so that gas will not evolve out of the sample. Alternatively, because knowledge of the exact dew point of a retrograde gas condensate in a formation is desirable, a decision may be made, when conditions allow, to vary the pressure drawdown in an attempt to observe the liquid condensation and thus establish the actual saturation pressure.

FIG. 1B illustrates an exemplary embodiment of the fluid analysis module **25** of FIG. 1A (labeled **25'**), including a probe **202** having a port **204** to admit formation fluid therein. A hydraulic extending mechanism **206** may be driven by a hydraulic system **220** to extend the probe **202** to sealingly engage the formation **14**. In alternative implementations, more than one probe can be used or inflatable packers can replace the probe(s) and function to establish fluid connections with the formation and sample fluid samples.

The probe **202** can be realized by the Quicksilver Probe offered by Schlumberger Technology Corporation of Sugar Land, Tex., USA. The Quicksilver Probe divides the fluid flow from the reservoir into two concentric zones, a central zone isolated from a guard zone about the perimeter of the central zone. The two zones are connected to separate flowlines with independent pumps. The pumps can be run at different rates to exploit filtrate/fluid viscosity contrast and permeability anisotropy of the reservoir. Higher intake velocity in the guard zone directs contaminated fluid into the guard zone flowline, while clean fluid is drawn into the central zone. Fluid analyzers analyze the fluid in each flowline to determine the composition of the fluid in the respective flowlines. The pump rates can be adjusted based on such compositional analysis to achieve and maintain desired fluid contamination levels. The operation of the Quicksilver Probe efficiently separates contaminated fluid from cleaner fluid early in the fluid extraction process, which results in obtaining clean, fluid in much less time than traditional formation testing tools.

The fluid analysis module **25'** includes a flowline **207** that carries formation fluid from the port **204** through a fluid analyzer **208**. The fluid analyzer **208** includes a light source that directs light to a sapphire prism disposed adjacent the flowline fluid flow. The reflection of such light is analyzed by a gas refractometer and dual fluoroscence detectors. The gas refractometer qualitatively identifies the fluid phase in the flowline. At the selected angle of incidence of the light emitted from the diode, the reflection coefficient is much larger when gas is in contact with the window than when oil or water is in contact with the window. The dual fluoroscence detectors detect free gas bubbles and retrograde liquid dropout to accurately detect single-phase fluid flow in the flowline **207**. Fluid type is also identified. The resulting phase information can be used to define the difference between retrograde condensates and volatile oils, which can have similar GORs and live-oil densities. It can also be used to monitor phase separation in real time and ensure single-phase sampling. The fluid analyzer **208** also includes dual spectrometers—a filter-array spectrometer and a grating-type spectrometer.

The filter-array spectrometer of the analyzer **208** includes a broadband light source providing broadband light that passes along optical guides and through an optical chamber in the flowline to an array of optical density detectors that are designed to detect narrow frequency bands (commonly referred to as channels) in the visible and near-infrared spectra as described in U.S. Pat. No. 4,994,671, herein incorporated by reference in its entirety. Preferably, these channels include a subset of channels that detect water absorption peaks (which are used to characterize water content in the fluid) as well as a dedicated channel corresponding to the

absorption peak of CO₂ with dual channels above and below this dedicated channel that subtract out the overlapping spectrum of hydrocarbon and small amounts of water (which are used to characterize CO₂ content in the fluid). The filter array spectrometer also employs optical filters that, provide for identification of the color (also referred to as “optical density” or “OD”) of the fluid in the flowline. Such color measurements support fluid identification, determination of asphaltene content, and pH measurement. Mud filtrates or other solid materials generate noise in the channels of the filter array spectrometer. Scattering caused by these particles is Independent of wavelength. In the preferred embodiment, the effect of such scattering can be removed by subtracting a nearby channel.

The grating-type spectrometer of the analyzer **208** is designed to detect channels in the near-infrared spectra (preferably 1600-1800 nm) where reservoir fluid has absorption characteristics that reflect molecular structure.

The analyzer **208** also includes a pressure sensor for measuring pressure of the formation fluid in the flowline **207**, a temperature sensor for measuring temperature of the formation fluid in the flowline **207**, and a density sensor for measuring five fluid density of the fluid in the flowline **207**. In the preferred embodiment, the density sensor is realized by a vibrating sensor that oscillates in two perpendicular modes within the fluid. Simple physical models describe the resonance frequency and quality factor of tire sensor in relation to live fluid density. Dual mode oscillation is advantageous over other resonant techniques because it minimizes the effects of pressure and temperature on the sensor through common mode rejection. In addition to density, the density sensor can also provide a measurement of live fluid viscosity from tire quality factor of oscillation frequency. Note that live fluid viscosity can also be measured by placing a vibrating object, in the fluid flow and measuring tire increase in line width of any fundamental resonance. This increase in line width is related closely to the viscosity of the fluid. The change in frequency of the vibrating object is closely associated with the mass density of the object. If density is measured independently, then the determination of viscosity is more accurate because the effects of a density change on the mechanical resonances are determined. Generally, the response of the vibrating object is calibrated against known standards. The analyzer **208** can also measure resistivity and pH of fluid in the flowline **207**. In the preferred embodiment, the fluid analyzer **208** is realized by the Insitu Fluid Analyzer available from Schlumberger Technology Corporation. In other exemplary implementations, the flowline sensors of the analyzer **208** may be replaced or supplemented with other types of suitable measurement sensors (e.g., NMR sensors, capacitance sensors, etc.). Pressure sensor(s) and/or temperature sensor(s) for measuring pressure and temperature of fluid drawn into the flowline **207** can also be part of the probe **202**.

A pump **228** is fluidly coupled to the flowline **207** and is controlled to draw formation fluid into the flowline **207** and possibly to supply formation fluid to the fluid collecting chambers **22** and **23** (FIG. 1A) via valve **229** and flowpath **231** (FIG. 1B).

The fluid analysis module **25'** includes a data processing system **213** that receives and transmits control and data signals to the other components of the module **25'** for controlling operations of the module **25'**. The data processing system **213** also interfaces to the fluid analyzer **208** for receiving, storing and processing the measurement data generated therein. In the preferred embodiment, the data processing system **213** processes the measurement data output by the fluid analyzer

208 to derive and store measurements of the hydrocarbon composition of fluid samples analyzed insitu by the fluid analyzer 208, including

- flowline temperature;
- flowline pressure;
- optical density;
- live fluid density (ρ) at the flowline temperature and pressure;
- live fluid viscosity (μ) at flowline temperature and pressure;
- concentrations (e.g., weight percentages) of carbon dioxide (CO_2), methane (CH_4), ethane (C_2H_6), the C3-C5 alkane group, the lump of hexane and heavier alkane components (C6+), and asphaltene content;
- GOR; and
- possibly other parameters (such as API gravity, oil formation volume factor (Bo), etc.)

Flowline temperature and pressure are measured by the temperature sensor and pressure sensor, respectively, of the fluid analyzer 208 (and/or probe 202). In the preferred embodiment, the output of the temperature sensor(s) and pressure sensor(s) are monitored continuously before, during, and after sample acquisition to derive the temperature and pressure of the fluid in the flowline 207. The formation temperature is not likely to deviate substantially from the flowline temperature at a given measurement station and thus can be estimated as the flowline temperature at the given measurement station in many applications. Formation pressure can be measured by the pressure sensor of the fluid analyzer 208 in conjunction with the downhole fluid sampling and analysis at a particular measurement station after buildup of the flowline to formation pressure.

Live fluid density (ρ) at the flowline temperature and pressure is determined by the output of the density sensor of the fluid analyzer 208 at the time the flowline temperature and pressure are measured.

Live fluid viscosity (μ) at flowline temperature and pressure is derived from the quality factor of the density sensor measurements at the time the flowline temperature and pressure are measured.

The measurements of the hydrocarbon composition of fluid samples are derived by translation of the data output by spectrometers of the fluid analyzer 208.

The GOR is determined by measuring the quantity of methane and liquid components of crude oil using near infrared absorption peaks. The ratio of the methane peak to the oil peak on a single phase live crude oil is directly related to GOR.

The fluid analysis module 25' can also detect and/or measure other fluid properties of a given live oil sample, including retrograde dew formation, asphaltene precipitation, and/or gas evolution.

The fluid analysis module 25' also includes a tool bus 214 that communicates data signals and control signals between the data processing system 213 and the surface-located system 18 of FIG. 1A. The tool bus 214 can also carry electrical power supply signals generated by a surface-located power source for supply to the module 25', and the module 25' can include a power supply transformer/regulator 215 for transforming the electric power supply signals supplied via the tool bus 214 to appropriate levels suitable for use by the electrical components of the module 25'.

Although the components of FIG. 1B are shown and described above as being communicatively coupled and arranged in a particular configuration, persons of ordinary skill in the art will appreciate that the components of the fluid analysis module 25' can be communicatively coupled and/or

arranged differently than depicted in FIG. 1B without, departing from the scope of the present disclosure. In addition, the example methods, apparatus, and systems described herein are not limited to a particular conveyance type but, instead, may be implemented in connection with different conveyance types including, for example, coiled tubing, wireline, wired drill pipe, and/or other conveyance means known in the industry.

In accordance with the present invention, the system of FIGS. 1A and 1B can be employed with the methodology of FIGS. 2A-2G to characterize the fluid properties of a petroleum reservoir of interest based upon downhole fluid analysis of samples of reservoir fluid. As will be appreciated by those skilled in the art, the surface-located electrical control system 18 and the fluid analysis module 25 of the tool 10 each include data processing functionality (e.g., one or more microprocessors, associated memory, and other hardware and/or software) that cooperate to implement the invention as described herein. The electrical control system 18 can also be realized by a distributed data processing system wherein data measured by the tool 10 is communicated in real time over a communication link (typically a satellite link) to a remote location for data analysis as described herein. The data analysis can be carried out on a workstation or other suitable data processing system (such as a computer cluster or computing grid).

The fluid analysis of FIGS. 2A-2G relies on a solubility model to characterize relative concentrations of high molecular weight fractions (resins and/or asphaltenes) as a function of depth in the oil column as related to relative solubility, density and molar volume of such high molecular weight fractions (resins and/or asphaltenes) at varying depth. In the preferred embodiment, the solubility model treats the reservoir fluid as a mixture (solution) of two parts: a solute part (resins and/or asphaltenes) and a solvent part (the lighter components other than resins and asphaltenes). The solute part is selected from a number of classes that include resins, asphaltene nanoaggregates, asphaltene clusters, and combinations thereof. For example, one class can include resins with little or no asphaltene nanoaggregates and asphaltene clusters. Another class can include asphaltene nanoaggregates with little or no resins and asphaltene clusters. A further class can include resins and asphaltene nanoaggregates with little or no asphaltene clusters. A further class can include asphaltene clusters with little or no resins and asphaltene nanoaggregates. The solvent part is a mixture whose properties are measured by downhole fluid analysis and/or estimated by the EOS model. It is assumed that the reservoir fluids are connected (i.e., there is a lack of compartmentalization) and in thermodynamic equilibrium. In this approach, the relative, concentration (volume fraction) of the solute part as a function of depth is given by:

$$\frac{\phi_i(h_2)}{\phi_i(h_1)} = \exp \left\{ \frac{v_i g (\rho_m - \rho_i) (h_2 - h_1)}{RT} + \left(\frac{v_i}{v_m} \right)_{h_2} - \left(\frac{v_i}{v_m} \right)_{h_1} - \frac{v_i [(\delta_i - \delta_m)_{h_2}^2 - (\delta_i - \delta_m)_{h_1}^2]}{RT} \right\} \quad (1)$$

where

- $\phi_i(h_1)$ is the volume fraction for the solute part at depth h_1 ,
- $\phi_i(h_2)$ is the volume fraction for the solute part at depth h_2 ,
- v_i is the partial molar volume for the solute part,
- v_m is the molar volume for the solution,
- δ_i is the solubility parameter for the solute part,

δ_m is the solubility parameter for the solution,
 ρ_i is the partial density for the solute part,
 ρ_m is the density for the solution,
 R is the universal gas constant,
 T is the absolute temperature of the reservoir fluid, and
 g is the gravitational constant.

In Eq. 1 it is assumed that properties of the solute part (resins and asphaltenes) are independent of depth. For properties of the solution that are a function of depth, average values are used between the two depths, which does not result in a loss of computational accuracy. Further, if the concentrations of resins and asphaltenes are small, the properties of the solute and solvent parts (the solution) with subscript m approximate those of the solvent part. The first exponential term of Eq. (1) arises from gravitational contributions. The second and third exponential terms arise from the combinatorial entropy change of mixing. The fourth exponential term arises from the enthalpy (solubility) change of mixing. It can be assumed that the reservoir fluid is isothermal. In this case, the temperature T can be set to the average formation temperature as determined from downhole fluid analysis. Alternatively, a temperature gradient with depth (preferably a linear temperature distribution) can be derived from downhole fluid analysis and the temperature T at a particular depth determined from such temperature gradient.

The density ρ_m of the solution at a given depth can be derived from the partial densities of the components of the solution at the given depth by:

$$\rho_m = \sum_j \rho_j \phi_j \quad (2)$$

where

ϕ_j is the volume fraction of the component j of the solution at the given depth, and

ρ_j is the partial density for the component j of the solution at the given depth.

The volume fractions ϕ_j for the components of the solution at the given depth can be measured, estimated from measured mass or mole fractions, estimated from the solution of the compositional gradients produced by the EOS model, or other suitable approach.

The molar volume v_m for the solution at a given depth can be derived by:

$$v_m = \frac{\sum_j x_j m_j}{\rho_m} \quad (3)$$

where

x_j is the mole fraction of component j of the solution,

m_j is the molar mass of component j of the solution, and

ρ_m is the density of the solution.

The mole fractions x_j at the given depth can be measured, estimated from measured mass or mole fractions, estimated from the solution of the compositional gradients produced by the EOS model, or other suitable approach. The molar mass m_j for the components of the solvent part are known. The density ρ_m for the solution at the given depth is provided by the solution of Eq. (2).

The solubility parameter δ_m for the solution at a given depth can be derived as the average of the solubility parameters for the components of the solution at the given depth, given by:

$$\delta_m \left(\frac{\sum_i \phi_i \delta_i}{\sum_j \phi_j} \right) \quad (4)$$

where

ϕ_j is the volume fraction of the component j of the solution at the given depth, and

δ_j is the solubility parameter for the component j of the solution at the given depth.

The volume fractions ϕ_j at the given depth can be measured, estimated from measured mass or mole fractions, estimated from the solution of the compositional gradients produced by the EOS model, or other suitable approach. The solubility parameters δ_j at the given depth can be known, or estimated from measured mass or mole fractions, estimated from the solution of the compositional gradients produced by the EOS model, or other suitable approach.

It is also contemplated that the solubility parameter δ_m for the solution at a given depth can be derived from an empirical correlation to the density ρ_m of the solution at a given depth. For example, the solubility parameter δ_m (in $(\text{MPa})^{0.5}$) can be derived from:

$$\delta_m = D \rho_m + C \quad (5)$$

where

$D = (0.00487 R_s + 9.10199)$,

$C = (8.3271 \rho_m - 0.004878 R_s \rho_m + 2.904)$,

R_s is the GOR at the given depth in scf/STB, and

ρ_m is the bulk live oil density at the given depth in g/cm^3 .

The GOR (R_s) as a function of depth in the oil column can be measured by downhole fluid analysis or derived from the predictions of compositional components of the reservoir fluid as a function of depth as described below. The bulk live oil density (ρ_m) as a function of depth can be measured by downhole fluid analysis or derived from the predictions of compositional components of the reservoir fluid as a function of depth. In another example, the solubility parameter δ_m (in $(\text{MPa})^{0.5}$) can be derived from a simple correlation to the density ρ_m of the solution at a given depth (in g/cm^3) given by:

$$\delta_m = 17.347 \rho_m + 2.904 \quad (6)$$

The solubility parameter (in $(\text{MPa})^{0.5}$) of the solute part can be derived from a given temperature gradient relative to a reference measurement station ($\Delta T = T - T_0$) by:

$$\delta_i(T) = \delta_i(T_0) [1 - 1.07 \times 10^{-3} (\Delta T)] \quad (7)$$

where

T_0 is the temperature at the reference measurement station (e.g., $T_0 = 298.15 \text{ K}$), and

$\delta_i(T_0)$ is a solubility parameter (in $(\text{MPa})^{0.5}$) for the solute part at T_0

(e.g., $\delta_i(T_0) = 20.5 \text{ MPa}^{0.5}$ for the class where the solute part includes resins (with little or no asphaltene nanoaggregates or asphaltene clusters), and $\delta_i(T_0) = 21.85 \text{ MPa}^{0.5}$ for those classes where the solute part includes asphaltenes (such as classes that include asphaltene nanoaggregates, asphaltene clusters and asphaltene nanoaggregate/resin combinations). The impact of pressure on the solubility parameter for the solute part is small and negligible.

The partial density (in kg/m^3) of the solute part can be derived from constants, such as 1.15 kg/m^3 for the class where the solute part, includes resins (with little or no asphaltene nanoaggregates or asphaltene clusters), and 1.2 kg/m^3 for those classes where the solute part includes asphaltenes (such as classes that include asphaltene nanoaggregates, asphaltene clusters and asphaltene nanoaggregate/resin combinations).

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Other types of functions can be employed to correlate the properties of the solute part as a function of depth. For example, a linear function of the form of Eq. (8) can be used, to correlate a property of the solution (such as partial density and solubility parameter) as a function of depth

$$\alpha = c\Delta h + \alpha_{ref} \quad (8)$$

where

α is the property (such as partial density and solubility parameter) of the solution,

c is a coefficient,

α_{ref} is the property of the solution at a reference depth, and Δh is the difference in height relative to the reference depth.

Once the properties noted above are obtained, the remaining adjustable parameter in Eq. (1) is the molar volume of the solute part. The molar volume of the solute part, varies for the different classes. For example, resins have a smaller molar volume than asphaltene nanoaggregates, which have a smaller molar volume than asphaltene clusters. The model assumes that the molar volume of the solute part is constant as function of depth. A spherical model is preferably used to estimate the molar volume of the solute, part by:

$$V = 1/6 * \pi * d^3 * N_a \quad (9)$$

where V is the molar volume, d is the molecular diameter, and N_a is Avogadro's constant.

For example, for the class where the solute part includes resins (with little or no asphaltene nanoaggregates and asphaltene clusters), the molecular diameter d can vary over a range of 1.25 ± 0.15 nm. For the class where the solute part includes asphaltene nanoaggregates (with little or no resins and asphaltene clusters), the molecular diameter d can vary over a range of 1.8 ± 0.2 nm. For the class where the solute part includes asphaltene clusters (with little or no resins and asphaltene nanoaggregates), the molecular diameter d can vary over a range of 4.5 ± 0.5 nm. For the class where the solute part is a mixture of resins and asphaltene nanoaggregates (with little or no asphaltene clusters), the molecular diameter d can vary over the range corresponding to such resins and nanoaggregates (e.g., between 1.25 nm and 1.8 nm). These diameters are exemplary in nature and can be adjusted as desired.

In this manner, Eq. (1) can be used to determine a family of curves for each solute part class. The family of curves represents an estimation of the concentration of the solute part class part as a function of depth. Each curve of the respective family is derived from a molecular diameter d that falls within the range of diameters for the corresponding solute part class. A solution can be solved by fitting the curves to corresponding measurements of the concentration of the respective solute part class at varying depths as derived from downhole fluid analysis to determine the best matching curve. For example, the family of curves for the solute part class including resins (with little or no asphaltene nanoaggregates and clusters) can be fit to measurements of resin concentrations at varying depth. In another example, the family of curves for the solute part class including asphaltene nanoaggregates (with little or no resins and asphaltene clusters) can be fit to measurements of asphaltene nanoaggregate concentrations at varying depth. In still another example, the family of curves for the solute part class including asphaltene clusters (with little or no resins and asphaltene nanoaggregates) can be fit to measurements of asphaltene cluster concentrations at varying depth. In yet another example, the family of curves for the solute part class including resins and asphaltene nanoaggregates (with little or no asphaltene clusters) can be fit to measurements of mixed resins and asphaltene nanoaggregate

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concentrations at varying depth. If a best fit is identified, the estimated and/or measured properties of the best matching solute class (or other suitable properties) can be used for reservoir analysis. If no fit is possible, then the reservoir fluids might not be in equilibrium or a more complex formulation may be required to describe the petroleum fluid in the reservoir.

Other suitable structural models can be used to estimate and vary the molar volume for the different solute part classes. It is also possible that Eq. (1) can be simplified by ignoring certain exponent terms, which gives an analytical model of the form:

$$\frac{\phi_i(h_2)}{\phi_i(h_1)} = \exp\left\{\frac{v_i g(\rho_m - \rho_i)(h_2 - h_1)}{RT}\right\} \quad (10)$$

This Eq. (10) can be solved in a manner similar to that described above for Eq. (1) in order to derive the relative concentration of solute part as a function of depth (h) in the reservoir.

The operations of FIGS. 2A-2G begin in step 201 by employing the downhole fluid analysis (DFA) tool of FIGS. 1A and 1B to obtain a sample of the formation fluid at the reservoir pressure and temperature (a live oil sample) at a measurement station in the wellbore (for example, a reference station). The sample is processed by the fluid analysis module 25. In the preferred embodiment, the fluid analysis module 25 performs spectrophotometry measurements that measure absorption spectra of the sample and translates such spectrophotometry measurements into concentrations of several alkane components and groups in the fluids of interest. In an illustrative embodiment, the fluid analysis module 25 provides measurements of the concentrations (e.g., weight percentages) of carbon dioxide (CO_2), methane (CH_4), ethane (C_2H_6), the C3-C5 alkane group including propane, butane, pentane, the lump of hexane and heavier alkane components (C6+), and asphaltene content. The tool 10 also preferably provides a means to measure temperature of the fluid sample (and thus reservoir temperature at the station), pressure of the fluid sample (and thus reservoir pressure at the station), optical density of the fluid sample, live fluid density of the fluid sample, live fluid viscosity of the fluid sample, gas-oil ratio (GOR) of the fluid sample, optical density, and possibly other fluid parameters (such as API gravity, formation volume fraction (FVF), etc.) of the fluid sample.

In step 203, a delumping process is carried out to characterize the compositional components of the sample analyzed in 201. The delumping process splits the concentration (e.g., mass fraction, which is sometimes referred to as weight fraction) of given compositional lumps (C3-C5, C6+) into concentrations (e.g., mass fractions) for single carbon number (SCN) components of the given compositional lump (e.g., split C3-C5 lump into C3, C4, C5, and split C6+ lump into C6, C7, C8...). The exemplary delumping operations carried out as part of step 203 are described in detail in U.S. Patent Application Publication 2009/0192768, herein incorporated by reference in its entirety.

In step 205, the results of the delumping process of step 203 are used in conjunction with an equation of state (EOS) model to predict compositions and fluid properties (such as volumetric behavior of oil and gas mixtures) as a function of depth in the reservoir. In the preferred embodiment, the predictions of step 205 include property gradients, pressure gradients, and temperature gradients of the reservoir fluid as a function of depth. The property gradients preferably include mass

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fractions, mole fractions, molecular weights and specific gravities for a set of SCN components (but not for asphalt-
enes) as a function of depth in the reservoir. The property
gradients predicted in step 205 preferably do not include
compositional gradients (i.e., mass fractions, mole fractions,
molecular weights and specific gravities) specifically for res-
ins and asphaltenes as a function, of depth, as such analysis is
provided by a solubility model as described herein in more
detail. The variations of fluid properties with depth represent
the variations of the hulk fluid (solution) properties, although
resins and asphaltenes are not specifically treated.

The EOS model of step 205 includes a set of equations that
represent the phase behavior of the compositional compo-
nents of the reservoir fluid. Such equations can take many
forms. For example, they can be any one of many cubic EOS,
as is well known. Such cubic EOS include van der Waals EOS
(1873), Redlich-Kwong EOS (1949), Soave-Redlich-Kwong
EOS (1972), Peng-Robinson EOS (1976), Stryjek-Vera-
Peng-Robinson EOS (1986) and Patel-Teja EOS (1982). Vol-
ume shift parameters can be employed as part of the cubic
EOS in order to improve liquid density predictions, as is well
known. Mixing rules (such as van der Waals mixing rule) can
also be employed as part of the cubic EOS, A SAFT-type EOS
can also be used, as is well known in the art. In these equa-
tions, the deviation from the Ideal gas law is largely
accounted for by introducing (1) a finite (non-zero) molecular
volume and (2) some molecular interaction. These param-
eters are then related to the critical constants of the different
chemical components.

In the preferred embodiment, the EOS model of step 205
predicts compositional gradients with depth that take into
account, the impacts of gravitational forces, chemical forces,
thermal diffusion, etc. To calculate compositional gradients
with depth in a hydrocarbon reservoir, it is usually assumed
that the reservoir fluids are connected (i.e., there is a lack of
compartmentalization) and in thermodynamic equilibrium
(with no adsorption phenomena or any kind of chemical
reactions in the reservoir). The mass flux (J) of compositional
component i that crosses the boundary of an elementary vol-
ume of the porous media is expressed as:

$$J_i = \rho_i \left(\sum_{j=1}^n (L_{ij} \nabla_r g_j^i) + L_{ip} (\rho g - \nabla P) + L_{iq} \nabla T \right) \quad (11)$$

where

L_{ij} , L_{ip} , and L_{iq} are the phenomenological coefficients,
 ρ_i denotes the partial density of component i,
 ρ , g , P , T are the density, the gravitational acceleration,
pressure, and temperature, respectively, and
 g_j^i is the contribution of component j to mass free energy of
the fluid in a porous media, which can be divided into a
chemical potential part μ_i and a gravitational part gz
(where z is the vertical depth).

The average fluid velocity (u) is estimated by:

$$u = \frac{\sum_{j=1}^n J_j}{\rho} \quad (12)$$

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According to Darcy's law, the phenomenological baro-
diffusion coefficients must meet the following constraint:

$$\frac{k}{\eta} = \frac{\sum_{j=1}^n \rho_j L_{jp}}{\rho} \quad (13)$$

where k and η are the permeability and the viscosity,
respectively.

If the pore size is far above the mean free path of molecules,
the mobility of the components, due to an external pressure
field, is very close to the overall mobility. The mass chemical
potential is a function of mole fraction (x), pressure, and
temperature.

At constant temperature, the derivative of the mass chemi-
cal potential (μ_i) has two contributions:

$$\nabla_T \mu_j = \sum_{k=1}^n \left(\frac{\partial \mu_j}{\partial x_k} \right)_{T,P,x_{1 \neq k}} \nabla x_k + \left(\frac{\partial \mu_j}{\partial P} \right)_{T,x} \nabla P \quad (14)$$

where the partial derivatives can be expressed in terms of EOS
(fugacity coefficients):

$$\left(\frac{\partial \mu_j}{\partial x_k} \right)_{T,P,x_{j \neq k}} = \frac{RT}{M_j} \left(\frac{\partial \ln f_j}{\partial x_k} \right)_{T,P,x_{j \neq k}} = \frac{RT}{M_j} \left(\frac{\delta_{jk}}{x_k} + \frac{1}{\phi_j} \left(\frac{\partial \phi_j}{\partial x_k} \right)_{T,P,x_{j \neq k}} \right) \quad (15)$$

$$\left(\frac{\partial \mu_j}{\partial P} \right)_{T,x} = \frac{\bar{v}_j}{M_j} = \frac{RT}{M_j} \left(\frac{1}{P} + \left(\frac{\partial \phi_j}{\partial P} \right)_{T,x} \right) \quad (16)$$

where M_j , f_j , ϕ_j , and \bar{v}_j are the molecular mass, fugacity,
fugacity coefficient, and partial molar volume of component
j, respectively;

x_k is the mole fraction of component k;

R denotes the universal gas constant; and

δ is the Kronecker delta function.

In the ideal case, the phenomenological coefficients (L)
can be related to effective practical diffusion coefficients
(D_i^{eff}).

$$L_{ii} = - \frac{M_i}{RT} D_i^{eff} \quad (17)$$

The mass conservation for component i in an n-component
reservoir fluid, which governs the distribution of the compo-
nents in the porous media, is expressed as:

$$\frac{\partial \rho_i}{\partial t} + \nabla J_i = 0, \quad i = 1, 2, \dots, n. \quad (18)$$

The equation can be used to solve a wide range of problems.
This is a dynamic model which is changing with time t.

Let us consider that the mechanical equilibrium of the fluid
column has been achieved:

$$\nabla_z P = \rho g \quad (19)$$

The vertical distribution of the components can be calculated by solving the following set of equations;

$$\frac{\partial \ln f_i}{\partial z} - \frac{M_i g}{RT} + \frac{J_{i,z}}{x_i D_i^{\text{eff}}} \frac{M}{\rho M_i} - \frac{L_{iq}}{D_i^{\text{eff}}} \frac{\partial T}{\partial z} = 0, \quad i = 1, 2, \dots, n \quad (20)$$

$$\sum_{k=1}^n \left(\frac{\delta_{ik}}{x_k} + \frac{1}{\varphi_i} \frac{\partial \varphi_i}{\partial x_k} \right) \nabla_z x_k + \frac{(v_i \rho - M_i) g}{RT} + \frac{J_{i,z}}{x_i D_i^{\text{eff}}} \frac{M}{\rho M_i} - \frac{L_{iq}}{D_i^{\text{eff}}} \frac{\partial T}{\partial z} = 0 \quad (21)$$

where $J_{i,z}$ is the vertical component, of the external mass flux and M is the average molecular mass. This formulation allows computation of the stationary state of the fluid column and it does not require modeling of the dynamic process leading to the observed compositional distribution.

If the horizontal components of external fluxes are significant, the equations along the other axis have to be solved as well. Along a horizontal "x" axis the equations become:

$$\frac{\partial \ln f_i}{\partial x} + \frac{J_{i,x}}{x_i D_i^{\text{eff}}} \frac{M}{\rho M_i} - \frac{L_{iq}}{D_i^{\text{eff}}} \frac{\partial T}{\partial x} = 0. \quad (22)$$

The mechanical equilibrium of the fluid column $\nabla_z P = \rho g$, is a particular situation which will occur only in highly permeable reservoirs. In the general case, the vertical pressure gradient is calculated by:

$$\nabla_z P = \rho g - \frac{\nabla_z P_{\text{fluxes}} + \nabla_z P_{\text{Soret}}}{1 + R_p} \quad (23)$$

where R_p is calculated by

$$R_p = RT \frac{k}{\eta M} \sum_{i=1}^n \frac{x_i}{D_i^{\text{eff}}} \quad (24)$$

The pressure gradient contribution from thermal diffusion (so-called Soret contribution) is given by:

$$\nabla_z P_{\text{Soret}} = RT \frac{\rho}{M} \sum_{i=1}^n x_i \frac{L_{iq}}{D_i^{\text{eff}}} \nabla_z T. \quad (25)$$

And the pressure gradient contribution from external fluxes is expressed as

$$\nabla_z P_{\text{fluxes}} = RT \sum_{i=1}^n \frac{J_{i,z}}{M_i D_i^{\text{eff}}} \quad (26)$$

Assuming an isothermal reservoir and ignoring the external flux, results in the following equation;

$$\frac{\partial \ln f_i}{\partial z} - \frac{M_i g}{RT} = 0, \quad i = 1, 2, \dots, n. \quad (27)$$

Eq. (27) can be rewritten as

$$\frac{\partial \ln f_i}{\partial z} - \frac{M_i g}{RT} + a_i = 0, \quad i = 1, 2, \dots, n. \quad (28)$$

where a_i is computed by:

$$a_i = \frac{J_{i,z}}{x_i D_i^{\text{eff}}} \frac{M}{\rho M_i} - \frac{L_{iq}}{D_i^{\text{eff}}} \frac{\partial T}{\partial z}, \quad i = 1, 2, \dots, n. \quad (29)$$

The first part of the a_i term of Eq. (29) can be simplified to

$$\frac{J_{i,z}}{x_i \rho D_i^{\text{eff}}} \quad (30)$$

The second part of the a_i term of Eq. (29) can be written in the form proposed by Haase in "Thermodynamics of Irreversible Processes," Addison-Wesley, Chapter 4, 1969. In this manner, a_i is computed by:

$$a_i = \frac{J_{i,z}}{x_i \rho D_i^{\text{eff}}} + M_i \left(\frac{H_m}{M_m} - \frac{H_i}{M_i} \right) \frac{\Delta T}{T}, \quad i = 1, 2, \dots, n \quad (31)$$

where H_i is the partial molar enthalpy for component i , H_m is the molar enthalpy for the mixture, M_i is the molecular mass for component i , M_m is the molecular mass for the mixture, T is the formation temperature, and ΔT is the temperature difference between two vertical depths.

The first part of the a_i term of Eqs. (29) and (31) accounts for external fluxes in the reservoir fluid. It can be ignored if a steady state is assumed. The second part of the a_i term of Eqs. (29) and (31) accounts for a temperature gradient in the reservoir fluid. It can be ignored if an isothermal reservoir is assumed.

The fugacity f_i of component i at a given depth can be expressed as function of the fugacity coefficient and mole fraction for the component i and reservoir pressure (P) at the given depth as

$$f_i = \phi_i x_i P. \quad (32)$$

The mole fractions of the components at a given depth must further sum to 1 such that

$$\sum_{i=1}^N x_i = 1$$

at a given depth. Provided the mole fractions and the reservoir pressure and temperature are known at the reference station, these equations can be solved for mole fractions (as well as mass fractions), partial molar volumes and volume fractions for the reservoir fluid components as well as pressure and temperature as a function of depth. Flash calculations can solve for fugacities of components (including the asphalt- enes) that form at equilibrium. Details of suitable flash cal-

culations are described by Li in "Rapid Flash Calculations for Compositional Simulation," SPE Reservoir Evaluation and Engineering, October 2006, herein incorporated by reference in its entirety. The flash equations are based on a fluid phase equilibria model that finds the number of phases and the distribution of species among the phases, that minimizes Gibbs Free Energy. More specifically, the flash calculations calculate the equilibrium phase conditions of a mixture as a function of pressure, temperature and composition. The fugacities of the components derived from such flash calculations can be used to derive asphaltene content as a function of depth employing the equilibrium equations described in U.S. Patent Application Publication 2009/0235731, herein incorporated by reference in its entirety.

In step 205, the predictions of compositional gradient can be used to predict properties of the reservoir fluid as a function of depth (typically referred to as a property gradient), as is well known. For example, the predictions of compositional gradient can be used to predict bubble point pressure, dew point pressure, live fluid molar volume, molecular weight, gas-oil ratio, live fluid density, viscosity, stock tank oil density, and other pressure-volume-temperature (PVT) properties as a function of depth in the reservoir.

In step 207, the DFA tool 10 of FIGS. 1A and 1B is used to obtain a sample of the formation fluid at the reservoir pressure and temperature (a live oil sample) at another measurement station in the wellbore, and the downhole fluid analysis as described above with respect to step 201 is performed on this sample. In an illustrative embodiment, the fluid analysis module 25 provides measurements of the concentrations (e.g., weight percentages) of carbon dioxide (CO_2), methane (CH_4), ethane (C_2H_6), the C3-C5 alkane group including propane, butane, pentane, the lump of hexane and heavier alkane components (C6+), and asphaltene content. The tool 10 also preferably provides a means to measure temperature of the fluid sample (and thus reservoir temperature at the station), pressure of the fluid sample (and reservoir pressure at the station can be obtained from pretest), live fluid density of the fluid sample, live fluid viscosity of the fluid sample, gas-oil ratio (GOR) of the fluid sample, optical density, and possibly other fluid parameters (such as API gravity, formation volume fraction (FVF), etc.) of the fluid sample.

Optionally, in step 209 the EOS model of step 205 can be tuned based on a comparison of the compositional and fluid property predictions derived by the EOS model of step 205 and the compositional and fluid property analysis of the DFA tool in 207. Laboratory data can also be used to tune the EOS model. Such tuning typically involves selecting parameters of the EOS model in order to improve the accuracy of the predictions generated by the EOS model. EOS model parameters that can be tuned include critical pressure, critical temperature and acentric factor for single carbon components, binary interaction coefficients, and volume translation parameters. An example of EOS model tuning is described in Reyadh A. Almehaideb et al., "EOS tuning to model full field crude oil properties using multiple well fluid PVT analysis," Journal of Petroleum Science and Engineering, Volume 26, Issues 1-4, pp. 291-300, 2000, herein incorporated by reference in its entirety. In the event that the EOS model is tuned, the compositional and fluid property predictions of step 205 can be recalculated from the tuned EOS model.

In step 211, the predictions of compositional gradients generated in step 205 (or in step 209 in the event that the EOS is tuned) are used to derive solubility parameters of the solution (and possibly oilier property gradients or solubility model inputs) as a function of depth in the oil column. For example, the predictions of compositional gradients can be

used to derive the density of the solution (Eq. (2)), the molar volume of the solution (Eq. (3)), and the solubility parameter of the solution (Eq. (4) or (5)) as a function of depth.

In steps 213 to 219, the solute part is treated as a particular first-type class, for example a class where the solute part includes resins (with little or no asphaltene nanoaggregates and asphaltene clusters). This class generally corresponds to reservoir fluids that include condensates with very small concentration of asphaltenes. Essentially, tire high content of dissolved gas and light hydrocarbons create a poor solvent for asphaltenes. Moreover, the processes that generate condensates do not tend to generate asphaltenes. For this class, the operations rely on an estimate that the average spherical diameter of resins is 1.25 ± 0.15 nm and that resins impart color at a predetermined visible wavelength (e.g. 647 nm). The average, spherical diameter of 1.25 ± 0.15 nm corresponds to an average molecular weight of 740 ± 250 g/mol. Laboratory centrifuge data also has shown the spherical diameter of resins is ~ 1.3 nm. This is consistent with the results in the literature. It is believed that resins impart color in the shorter visible wavelength range due to their relatively small number of fused aromatic rings ("FARs") in polycyclic aromatic hydrocarbons ("PAHs"). In contrast, asphaltenes impart color in both the short visible wavelength range and the longer near-infrared wavelength range due to their relatively larger number of FARs in PAHs. Consequently, resins and asphaltenes impart color in the same visible wavelength range due to overlapping electronic transitions of the numerous PAHs in the oil. However, in the longer near-infrared wavelength range, the optical absorption is predominantly due to asphaltenes.

In step 215, a number of average spherical diameter values within the range of 1.25 ± 0.15 nm (e.g., $d=1.1$ nm, $d=1.2$ nm, $d=1.3$ nm and $d=1.4$ nm) are used to estimate corresponding molar volumes for the particular solute part class utilizing Eq. (9).

In step 217, the molar volumes estimated in step 215 are used in conjunction with the Flory-Huggins type model described above with respect to Eq. (1) to generate a family of curves that predict the concentration of the particular solute part class of step 213 as a function of depth in the reservoir.

In step 219, the family of curves generated in step 217 are compared to measurements of resin concentration at corresponding depths as derived from associated DFA color measurements at the predetermined visible wavelength (647 nm). The comparisons are evaluated to identify the diameter that best satisfies a predetermined matching criterion. In the preferred embodiment, the matching criterion determines that there are small differences between the resin concentrations as a function of depth as predicted by the Flory-Huggins type model and the corresponding resin concentrations measured from DFA analysis, thus providing an indication of a proper match within an acceptable tolerance level.

In steps 221 to 227, the solute part is treated as a particular second-type class, for example a class where the solute part includes asphaltene nanoaggregates (with little or no resins and asphaltene clusters). This class generally corresponds to low GOR black oils that usually have little compressibility. These types of black oils often contain asphaltene molecules with 4 to 7 FARs in PAHs. The asphaltene molecules are dispersed in the oil as nanoaggregates with an aggregation number of 2-8. For this class, the operations rely on an estimate that the average spherical diameter of asphaltene nanoaggregates is 1.8 ± 0.2 nm and that the asphaltene nanoaggregates impart color at a predetermined near-infrared (NIR) wavelength (e.g. 1070 nm). The average spherical diameter of 1.8 ± 0.2 nm corresponds to an average molecular weight of

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2200±700 g/mol. This is consistent with the results in the literature. Field and laboratory analysis have shown that asphaltene nanoaggregates impart color in both the visible wavelength range around 640 nm and the NIR wavelength range around 1070 nm. It is believed that the asphaltene nanoaggregates impart color in both the short visible wavelength range and the longer near-infrared wavelength range due to their relatively larger number of FARs in PAHs.

In step 223, a number of average spherical diameter values within the range of 1.8±0.2 nm (e.g., d=1.6 nm, d=1.7 nm, d=1.8 nm, d=1.9 nm and d=2.0 nm) are used to estimate corresponding molar volumes for the particular solute part class utilizing Eq. (9).

In step 225, the molar volumes estimated in step 223 are used in conjunction with the Flory-Huggins type model described above with respect to Eq. (1) to generate a family of curves that predict the concentration of the particular solute part class of step 221 as a function of depth in the reservoir.

In step 227, the family of curves generated in step 225 are compared to measurements of asphaltene nanoaggregate concentration at corresponding depths as derived from associated DFA color measurements at the predetermined NIR wavelength (1070 nm). The comparisons are evaluated to identify the diameter that best, satisfies a predetermined matching criterion. In the preferred embodiment, the matching criterion determines that there are small differences between the asphaltene nanoaggregate concentrations as a function of depth as predicted by the Flory-Huggins type model and the corresponding asphaltene nanoaggregate concentrations measured from DFA analysis, thus providing an indication of a proper match within an acceptable tolerance level.

In steps 229 to 235, the solute part is treated as a particular third-type class, for example a class where the solute part includes a combination of resins and asphaltene nanoaggregates (with little or no asphaltene clusters). This class generally corresponds to black oils that include a mixture of resins and asphaltene nanoaggregates. For this class, the operations rely on an estimate that the average spherical diameter of the mixed resins and asphaltene nanoaggregates varies linearly from 1.5±0.2 nm to 2.0±0.2 nm according to wavelength in a range between a visible wavelength (647 nm) and a NIR wavelength (1070 nm). This conforms to an assumption that the average molecular diameter for mixed resin and asphaltene nanoaggregates increases linearly with increasing wavelength due to the increasing importance of absorption from the asphaltene aggregates in the longer wavelength region. It is believed that the asphaltene nanoaggregate content (weight percent) contributing to color increases exponentially with increasing wavelength. In the preferred embodiment, the relationship between the average spherical diameter (d) and wavelength can be given by:

$$d = C1 * \text{Wavelength} + C2 \quad (33)$$

where C1 and C2 are constants.

C1 and C2 can be determined by solving the relation utilizing two diameter/wavelength combinations. For instance, a combination of d=1.5 nm at 647 nm wavelength and a combination of d=2.0 nm at 1070 nm wavelength can be used to solve for C1 and C2. In another example, a combination of d=1.3 nm at 647 nm wavelength and a combination of d=1.8 nm at 1070 nm wavelength can be used to solve for C1 and C2. In yet another example, a combination of d=1.7 nm at 647 nm wavelength and a combination of d=2.2 nm at 1070 nm wavelength can be used to solve for C1 and C2.

In step 231, a number of average spherical diameter values and wavelength combinations defined by the relationship of

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step 229 are used to estimate corresponding molar volumes for the particular solute part class utilizing Eq. (9).

In step 233, tire molar-volumes estimated in step 231 are used in conjunction with the Flory-Huggins type solubility model described above with respect to Eq. (1) to generate a family of curves that predict the concentration of the particular solute part class of step 229 as a function of depth in the reservoir. Each curve is associated with a particular average spherical diameter value and wavelength combination.

In step 235, the family of curves generated in step 233 are compared to measurements of mixed resins and asphaltene nanoaggregate concentrations at corresponding depths as derived from associated DFA color measurements at the wavelength of the given diameter/wavelength combination for the respective curve. The comparisons are evaluated to identify the diameter that best satisfies a predetermined matching criterion. In the preferred embodiment, the matching criterion determines that there are small differences between the mixed resin and asphaltene nanoaggregate concentrations as a function of depth as predicted by the Flory-Huggins type model and the corresponding mixed resin and asphaltene nanoaggregate concentrations measured from DFA analysis, thus providing an indication of a proper match within an acceptable tolerance level.

In steps 237 to 243, the solute part is treated as a particular fourth-type class, for example a class where the solute part includes asphaltene clusters. This class generally corresponds to black oils where the asphaltene gradient is very large in the oil column. This behavior implies that both asphaltene nanoaggregates and asphaltene clusters are suspended in the oil column. For this class, the operations rely on an estimate that the average spherical diameter of asphaltene clusters is 4.5±0.5 nm at a predetermined NIR wavelength (1070 nm). Field and laboratory analysis have shown that asphaltene clusters impart color in both the visible wavelength range around 640 nm and the NIR wavelength range around 1070 nm. It is believed that the asphaltene clusters impart color in both the short visible wavelength range and the longer NIR wavelength range due to their relatively larger number of FARs in PAHs.

In step 239, a number of average spherical diameter values within the range of 4.5±0.5 nm (e.g., d=4.0 nm, d=4.3 nm, d=4.5 nm, d=4.8 nm and d=5.0 nm) are used to estimate corresponding molar volumes for the particular solute part class utilizing Eq. (9).

In step 241, the molar volumes estimated in step 239 are used in conjunction with the Flory-Huggins type model described above with respect to Eq. (1) to generate a family of curves that predict the concentration of the particular solute part class of step 237 as a function of depth in the reservoir.

In step 243, the family of curves generated in step 241 are compared to measurements of asphaltene cluster concentration at corresponding depths as derived from associated DFA color measurements at the predetermined NIR wavelength (1070 nm). The comparisons are evaluated to identify the diameter that best satisfies a predetermined matching criterion. In the preferred embodiment, the matching criterion determines that there are small differences between the asphaltene cluster concentrations as a function of depth as predicted by the Flory-Huggins type model and the corresponding asphaltene cluster concentrations measured from DFA analysis, thus providing an indication of a proper match within an acceptable tolerance level.

In step 245, the matching diameters identified in steps 219, 227, 235 and 243 (if any) are evaluated to determine the best matching diameter of the group. The evaluation provides an indication of which particular solute part class (and thus the

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assumption of composition underlying the particular solute part class) is the best match to the measured gradient for the solvent part compositions.

In step 247, the result of the evaluation of step 245 is analyzed to determine if the best matching diameter corresponds to the solute part class of steps 213 to 219 where the solute part includes resins (with little or no asphaltene nanoaggregates and asphaltene clusters). If the answer is yes, the operations continue to step 249. Otherwise the operations continue to step 251.

In step 249, the workflow declares that the reservoir fluids are in thermal equilibrium within a non-compartmentalized reservoir, and the reservoir fluids include resins (with little or none asphaltene nanoaggregates or asphaltene clusters) in accordance with assumptions underlying the solute part class of steps 213 to 219. In this case, the reservoir fluid includes condensates with a very small concentration of asphaltenes. Essentially, the high content of dissolved gas and light hydrocarbons create a very poor solvent for asphaltenes. Moreover, processes that generate condensates do not tend to generate asphaltenes. Consequently, there is very little crude oil color as determined by DFA in the near-infrared range. Nevertheless, there are asphaltene like molecules—the resins—that absorb visible light and at times even some near infrared light. These resin molecules are largely dispersed in the condensate as molecules—thereby reducing the impact of the gravitational term. In addition, condensates exhibit considerable gradients. Since condensates are compressible, the hydrostatic head pressure of the condensate column generates a density gradient in the column. The density gradient creates the driving force to create a chemical composition gradient. The lower density components tend to rise in the column while the higher density components tend to settle down in the column. This GOR gradient gives rise to a large solubility contrast for the resins, thereby producing significant DFA color gradients. These gradients are useful to check for reservoir connectivity. Accordingly, the GOR gradient as determined by DFA analysis can be evaluated for reservoir analysis. The predicted and/or measured concentration of the resin component as a function of depth can also be evaluated for reservoir analysis. More specifically, connectivity can be indicated by moderately decreasing GOR values with depth, a continuous increase of resin content as a function of depth, and/or a continuous increase of fluid density and/or fluid viscosity as a function of depth. On the other hand, compartmentalization and/or non-equilibrium can be indicated by discontinuous GOR (or if lower GOR is found higher in the column), discontinuous resin content (or if higher asphaltene content is found higher in the column), and/or discontinuous fluid density and/or fluid viscosity (or if higher fluid density and/or fluid viscosity is found higher in the column).

In step 251, the result of the evaluation of step 245 is analyzed to determine if the best matching diameter corresponds to the solute part class of steps 221 to 227 where the solute part includes asphaltene nanoaggregates (with little or no resins and asphaltene clusters). If this is the case, the operations continue to step 253. Otherwise the operations continue to step 255.

In step 253, the workflow declares that the reservoir fluids are in thermal equilibrium within a non-compartmentalized reservoir, and the reservoir fluids include asphaltene nanoaggregates (with little or no resins and asphaltene clusters) in accordance with assumptions underlying the solute part class of steps 221 to 227 where the solute part includes asphaltene nanoaggregates (with little or no resins and asphaltene clusters). In this case, the predicted and/or measured concentration of the asphaltene nanoaggregates as a function of depth

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can be evaluated for reservoir analysis. More specifically, connectivity can be indicated by a continuous increase of asphaltene nanoaggregate content as a function of depth, and/or a continuous increase of fluid density and/or fluid viscosity as a function of depth. On the other hand, compartmentalization and/or non-equilibrium can be indicated by discontinuous asphaltene nanoaggregate content (or if higher asphaltene nanoaggregate content is found higher in the column), and/or discontinuous fluid density and/or fluid viscosity (or if higher fluid density and/or fluid viscosity is found higher in the column).

In step 255, the result of the evaluation of step 245 is analyzed to determine if the best matching diameter corresponds to the solute part class of steps 229 to 235 where the solute part includes a mix of resins and asphaltene nanoaggregates (with little or no asphaltene clusters). If this is the case, the operations continue to step 257. Otherwise the operations continue to step 259.

In step 257, the workflow declares that the reservoir fluids are in thermal equilibrium within a non-compartmentalized reservoir, and the reservoir fluids include a mixture of resins and asphaltene nanoaggregates (with little or no asphaltene clusters) in accordance with assumptions underlying the solute part class of steps 229 to 235 where the solute part includes a mixture of resins and asphaltene nanoaggregates (with little or no asphaltene clusters). In this case, the predicted and/or measured concentration of the mixture of resins and asphaltene nanoaggregates as a function of depth can be evaluated for reservoir analysis. More specifically, connectivity can be indicated by a continuous increase of the concentration of the resin/asphaltene nanoaggregate mixture as a function of depth, and/or a continuous increase of fluid density and/or fluid viscosity as a function of depth. On the other hand, compartmentalization and/or non-equilibrium can be indicated by discontinuous concentration of the resin/asphaltene nanoaggregate mixture (or if a higher concentration of the resin/asphaltene nanoaggregate mixture is found higher in the column), anchor discontinuous fluid density and/or fluid viscosity (or if higher fluid density and/or fluid viscosity is found higher in the column).

In step 259, the result of the evaluation of step 245 is analyzed to determine if the best matching diameter corresponds to the solute part class of steps 237 to 243 where the solute part includes asphaltene clusters. If this is the case, the operations continue to step 261. Otherwise the operations continue to step 263.

In step 261, the workflow declares that the reservoir fluids are in thermal equilibrium within a non-compartmentalized reservoir, and the reservoir fluids include asphaltene clusters in accordance with assumptions underlying the solute part class of steps 237 to 243 where the solute part includes asphaltene clusters. In this case, the predicted and/or measured concentration of the asphaltene clusters as a function of depth can be evaluated for reservoir analysis. More specifically, connectivity can be indicated by a continuous increase of asphaltene cluster content as a function of depth, and/or a continuous increase of fluid density and/or fluid viscosity as a function of depth. On the other hand, compartmentalization and/or non-equilibrium can be indicated by discontinuous asphaltene cluster content (or if higher asphaltene cluster content is found higher in the column), and/or discontinuous fluid density and/or fluid viscosity (or if higher fluid density and/or fluid viscosity is found higher in the column). Moreover, because asphaltene clusters are expected in the oil column, it is anticipated that:

large density and viscosity gradients exist in the oil column;

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the oil may have flow assurance problems (due to instability from e.g., the asphaltene onset pressure being equal to or greater than the formation pressure, or bitumens in the formation); and

there may be an allochthonous tar mat in the reservoir (as opposed to an autochthonous tar mat formed from biodegradation).

In step 263, no suitable match has been found between the solubility curves and the measured properties. In this case, the operations can determine if there is a need for additional measurement stations and/or different methodologies for repeat processing and analysis in order to improve the confidence level of the measured and/or predicted fluid properties. For example, the measured and/or predicted properties of the reservoir fluid can be compared to a database of historical reservoir data to determine whether the measured and/or predicted properties make sense. If the data does not make sense, additional measurement station(s) or different methodologies (e.g., different model(s)) can be identified for repeat processing and analysis in order to improve the confidence level of the measured and/or predicted fluid properties.

Other factors can be used to determine if there is a need for additional measurement stations and/or different methodologies for repeat processing and analysis in order to improve the confidence level of the measured and/or predicted fluid properties. For example, in step 263, it is expected that the reservoir is compartmentalized or not in thermodynamic equilibrium. Thus, the measured fluid properties can be accessed to confirm that they correspond to this expected architecture.

If in step 263 there is a need for additional measurement stations and/or different methodologies, the operations continue to step 265 to repeat the appropriate processing and analysis in order to improve the confidence level of the measured and/or predicted fluid properties.

If in step 263, there is no need for additional measurement stations and/or different methodologies (In other words, there is sufficient confidence level in the measured and/or predicted fluid properties), the operations continue to step 267 where the reservoir architecture is determined to be compartmentalized and/or not in thermodynamic equilibrium. Such a determination is supported by the invalidity of the assumptions of reservoir connectivity and thermal equilibrium that underlie the models utilized for predicting the solute part property gradient within file wellbore.

Subsequent to the determination of reservoir architecture in steps 249, 253, 257, 261, and 267, the results of such determination are reported to interested parties in step 269. The characteristics of the reservoir architecture reported in step 269 can be used to model and/or understand the reservoir of interest for reservoir assessment, planning, and management.

There have been described and illustrated herein a preferred embodiment of a method, system, and apparatus for downhole fluid analysis of the fluid properties of a reservoir of interest and for characterizing the reservoir of interest based upon such downhole fluid analysis. While particular embodiments of the invention have been described, it is not intended that the invention be limited thereto, as it is intended that, the invention be as broad in scope as the art will allow and that the specification be read likewise. Thus, while particular equations of state models, solubility models and applications of such models have been disclosed for predicting properties of reservoir fluid, it will be appreciated that other such models and applications thereof could be used as well. Moreover, the methodology described herein is not limited to stations in the same wellbore. For example, measurements from samples from different wells can be analyzed as described herein for

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testing for lateral connectivity. In addition, the workflow as described herein can be modified. For example, it is contemplated that user input can select the solute type classes from a list of solute type classes for processing. The user might also be able to specify certain parameters for the processing, such as diameters that are used as input to the solubility model to derive concentration curves for the relevant solute part classes, as well as optical density wavelengths that are used to correlate such concentrations to concentrations measured by downhole fluid analysis. It will therefore be appreciated by those skilled in the art that yet other modifications could be made to the provided invention without deviating from its scope as claimed.

What is claimed is:

1. A method for characterizing petroleum fluid in a reservoir traversed by at least one wellbore, the method comprising:

(a) at a plurality of measurements stations within the at least one wellbore, acquiring at least one fluid sample at the respective measurement station and performing downhole fluid analysis of the fluid sample using a fluid analysis module disposed in a borehole tool to measure properties of the fluid sample, the properties including concentration of a plurality of high molecular weight components, wherein the high molecular weight components are selected from the group including resins, asphaltene nanoaggregates, and asphaltene clusters;

(b) defining a plurality of type classes corresponding to different subsets of a predetermined set of high molecular weight components using a data processing system of the fluid analysis module, and using a model in the data processing system that predicts concentration of the high molecular weight components for each of the plurality of type classes and for said plurality of measurement stations, wherein for a number of different type class solute parts, the solubility model is used to generate a plurality of concentration curves corresponding to the respective type class solute part and a range of molar volumes associated with the respective type class solute part;

(c) comparing the predicted concentrations of the high molecular weight components for the plurality of type classes derived in (b) with corresponding concentrations measured by the downhole fluid analysis in (a) for said plurality of measurement stations to identify the best matching type class using the data processing system; and

(d) using the results of (c) for reservoir analysis and to adjust an operating parameter of the borehole tool based on the results of (c).

2. The method according to claim 1, wherein in (d), the results of (c) are used to determine reservoir architecture.

3. The method according to claim 1, wherein in (d), the results of (c) are used to identify predicted or measured properties that are to be evaluated to determine whether or not the reservoir is compartmentalized and/or in thermal equilibrium.

4. The method according to claim 1, wherein in (d), the results of (c) are used to determine whether or not to repeat the processing of (a) for one or more additional measurement stations.

5. The method according to claim 1, further comprising:

(e) inputting fluid sample properties measured in (a) to an equation of state model to predict compositional properties and fluid properties at different locations within the reservoir.

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6. The method according to claim 5, further comprising:
(f) tuning the equation of state model of (e) based on fluid sample properties measured in (a).

7. The method according to claim 5, wherein the equation of state model of (e) is used to derive inputs for the model of (b).

8. The method according to claim 1, wherein the model of (b) is a solubility model that characterizes relative concentrations of a set of high molecular weight components as a function of depth as related to relative solubility, density, and molar volume of the high molecular weight components of the set at varying depth.

9. The method according to claim 8, wherein the solubility model treats the reservoir fluid as a solution of two parts, the two parts being a solute part and a solvent part, the solute part comprising the set of high molecular weight components.

10. The method according to claim 9, wherein:

the model of (b) is based on a mathematical relationship of the form

$$\frac{\phi_i(h_2)}{\phi_i(h_1)} = \exp \left\{ \left(\frac{v_i g(\rho_m - \rho_i)(h_2 - h_1)}{RT} + \left(\frac{v_i}{v_m} \right)_{h_2} - \left(\frac{v_i}{v_m} \right)_{h_1} - \frac{v_i [(\delta_i - \delta_m)_{h_2}^2 - (\delta_i - \delta_m)_{h_1}^2]}{RT} \right) \right\}$$

where

$\phi_i(h_1)$ is the volume fraction for the solute part at depth h_1 ,

$\phi_i(h_2)$ is the volume fraction for the solute part at depth h_2 ,

v_i is the partial molar volume for the solute part,

v_m is the molar volume for the solution,

δ_i is the solubility parameter for the solute part,

δ_m is the solubility parameter for the solution part,

ρ_i is the partial density for the solute part,

ρ_m is the density for the solution,

R is the universal gas constant, and

T is the absolute temperature of the reservoir fluid.

11. The method according to claim 1, wherein the type class solute parts include a first-type class solute part that includes resins with little or no asphaltene nanoaggregates and asphaltene clusters.

12. The method according to claim 11, wherein the range of molar volumes associated with the first-type class solute part is derived from an average spherical diameter in a range of 1.25 ± 0.15 nm.

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13. The method according to claim 12, wherein in (c), the concentration curves for the first-type class solute part are compared to measurements of resin concentration derived from optical density measured from a predetermined visible wavelength around 647 nm.

14. The method according to claim 1, wherein the type class solute parts include a second type class solute part that includes asphaltene nanoaggregates with little or no resins and asphaltene clusters.

15. The method according to claim 14, wherein the range of molar volumes associated with the second-type class solute part is derived from an average spherical diameter in a range of 1.8 ± 0.2 nm.

16. The method according to claim 15, wherein in (c), the concentration curves for the second-type class solute part are compared to measurements of asphaltene nanoaggregate concentration derived from optical density measured from a predetermined near-infrared wavelength around 1070 nm.

17. The method according to claim 1, wherein the type class solute parts include a third-type class solute part that includes a mixture of resins and asphaltene nanoaggregates with little or no asphaltene clusters.

18. The method according to claim 17, wherein the range of molar volumes associated with the third-type class solute part is derived from an average spherical diameter in a range between 1.5 ± 0.2 nm and 2.0 ± 0.2 nm.

19. The method according to claim 18, wherein in (c), the concentration curves for the third-type class solute part are compared to measurements of mixed resins and asphaltene nanoaggregate concentration derived from optical density measured in a range between a visible wavelength around 647 nm and a near-infrared wavelength around 1070 nm.

20. The method according to claim 1, wherein the type class solute parts include a fourth-type class solute part that includes asphaltene clusters with little or no resins and asphaltene nanoaggregates.

21. The method according to claim 20, wherein the range of molar volumes associated with the fourth-type class solute part is derived from an average spherical diameter in a range of 4.5 ± 0.5 nm.

22. A method according to claim 21, wherein in (c), the concentration curves for the fourth-type class solute part are compared to measurements of asphaltene cluster concentration derived from optical density measured from a predetermined near-infrared wavelength around 1070 nm.

23. The method according to claim 1, wherein the high molecular weight components have an average molecular weight between 490 and 2900.

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